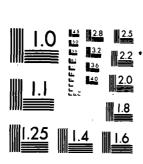
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MLS CHANNEL ASSIGNMENT MODEL

Thomas Hensler and Andrew Koshar
of
IIT Research Institute
Under Contract to
DEPARTMENT OF DEFENSE
Electromagnetic Compatibility Analysis Center
Annapolis, Maryland 21402



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AUGUST 1980

Interim Report

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Prepared for

U.S. DEPARTMENT OF TRANSPORTATION
FEDERAL AVIATION ADMINISTRATION
Systems Research & Development Service
Washington, D.C. 20590

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PREFACE

The Electromagnetic Compatibility Analysis Center (ECAC) is a Department of Defense facility, established to provide advice and assistance on electromagnetic compatibility matters to the Secretary of Defense, the Joint Chiefs of Staff, the military departments and other DoD components. The center, located at North Severn, Annapolis, Maryland 21402, is under policy control of the Assistant Secretary of Defense for Communication, Command, Control, and Intelligence and the Chairman, Joint Chiefs of Staff, or their designees, who jointly provide policy guidance, assign projects, and establish priorities. ECAC functions under the executive direction of the Secretary of the Air Force and the management and technical direction of the Center are provided by military and civil service personnel. The technical operations function is provided through an Air Force sponsored contract with the IIT Research Institute (IITRI).

This report was prepared for the Systems Research and Development Service of the Federal Aviation Administration in accordance with Interagency Agreement DOT-FA70WAI-175, as part of AF Project 649E under Contract F-19628-78-C-0006, by the staff of the IIT Research Institute at the Department of Defense Electromagnetic Compatibility Analysis Center.

To the extent possible, all abbreviations and symbols used in this report are taken from American Standards Y10.19 (1967) "Units Used in Electrical Science and Electrical Engineering" issued by the USA Standards Institute.

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FEDERAL AVIATION ADMINISTRATION SYSTEMS RESEARCH AND DEVELOPMENT SERVICE SPECTRUM MANAGEMENT STAFF

STATEMENT OF MISSION

The mission of the Spectrum Management Staff is to assist the Department of State, Office of Telecommunications Policy, and the Federal Communications Commission in assuring the FAA's and the nation's aviation interests with sufficient protected electromagnetic telecommunications resources throughout the world to provide for the safe conduct of aeronautical flight by fostering effective and efficient use of a natural resource—the electromagnetic radio-frequency spectrum.

This objective is achieved through the following services:

- Planning and defending the acquisition and retention of sufficient radio-frequency spectrum to support the aeronautical interests of the nation, at home and abroad, and spectrum standardization for the world's aviation community.
- Providing research, analysis, engineering, and evaluation in the development of spectrum related policy, planning, standards, criteria, measurement equipment, and measurement techniques.
- Conducting electromagnetic compatibility analyses to determine intra/inter-system viability and design parameters, to assure certification of adequate spectrum to support system operational use and projected growth patterns, to defend the aeronautical services spectrum from encroachment by others, and to provide for the efficient use of the aeronautical spectrum.
- Developing automated frequency-selection computer programs/routines to provide frequency planning, frequency assignment, and spectrum analysis capabilities in the spectrum supporting the National Airspace System.
- Providing spectrum management consultation, assistance, and guidance to all aviation interests, users, and providers of equipment and services, both national and international.

EXECUTIVE SUMMARY

The Federal Aviation Administration (FAA) has requested that the Electromagnetic Compatibility Analysis Center (ECAC) provide a channel-assignment model capable of making channel assignments for the new Microwave Landing System (MLS). The MLS consists of angle-guidance equipments operating in C-band and its associated Precision Distance Measurement Equipment (PDME) operating in L-band. It was desired that the model be capable of using various channel-separation criteria and assignment environments input by the user. It was also necessary that the model should assign equipments according to a user-input channelization scheme and be capable of pairing MLS and PDME channel assignments with existing TACAN/DME and VOR/ILS channels. The results of an assignment will be a list of the airport runways in the environment, the channel assigned to each runway, and an indication of which equipment contributed most to the failure of any runway to get a channel assigned.

The channel-assignment model consists of an intersite analysis routine and a channel assignment routine. The intersite analysis routine calculates desired-to-undesired signal power ratios (D/U) within each equipment's protected service volume. It then constructs an array containing the worst-case D/U value which exists between each pair of equipments in the environment.

The channel-assignment routine converts the worst-case D/U values to channel separation between equipments, and makes channel assignments that satisfy these separation requirements. The channel assignments are performed using a dynamic assignment technique in which the most difficult assignments (those with the least number of available channels) are attempted first. This routine includes an option allowing the user to specify the order of equipment assignment as he wishes, as an alternative to the dynamic technique.

A trial channel assignment of a Southwest U.S. airport environment using the dynamic ordering technique was made to test both the model and channel plan capability. This trial assignment is documented in the results section of this report.

FAA-RD-80-91

TABLE OF CONTENTS

Subsection	Page
SECTION 1	
INTRODUCTION	
BACKGROUND	1
OBJECTIVE	2
APPROACH	2
SECTION 2	
MODEL DESCRIPTION	
INTRODUCTION	6
INTERSITE ANALYSIS	7
Distance Cull	7
Minimum D/U Calculation	10
CHANNEL ASSIGNMENT	14
Denied Channel Array	14
Assignment	18
DATA BASE	20
Equipment Data	21
Facility Data	22
SECTION 3	
USER OPTIONS AND MODEL CAPABILITIES	
GENERAL	24
USER OPTION	24
Input Options	24
Model Options	. 31

TABLE OF CONTENTS (Continued)

Subsec	tion	Page
	SECTION 4	
	RESULTS	34
	LIST OF ILLUSTRATIONS	
Figure		
1	MLS CHANNEL ASSIGNMENT MODEL	6
2	INTERSITE LOGIC FLOW	8
3	DISTANCE CULL BOUNDARIES	9
4	TEST POINT LOCATIONS IN A SECTOR SERVICE VOLUME	11
5	COMPOSITE D/U _{ITS} CURVES FOR 5000-, 10,000- and 20,000-FOOT	
	ALTITUDES	13
6	ASSIGNMENT ROUTINE LOGIC FLOW	15
7	DENIED CHANNEL ARRAY CONSTRUCTION	17
8	CHANNEL-ASSIGNMENT PROCESS	19
9	DATA BASE RECORDS	30
	LIST OF TABLES	
Table		
1	SAMPLE L - BAND PROTECTION MATRIX IN dB	26
2	EXAMPLE CHANNEL PLAN	28
3	ALTERNATE PACKING ORDER	28
4	TRIAL ASSIGNMENT SUMMARY	34
	LIST OF APPENDIXES	
Appendi	ix	
Α	ANALYSIS APPROACH FOR DETERMINING MINIMUM D/U VALUES	A-1
В	SYSTEMS DESCRIPTIONS	B-1
С	EQUIPMENT PROTECTION CRITERIA	C-1
D	TRIAL ENVIRONMENT	D-1
E	CHANNEL PLAN	E-1
REFER	RENCES	R-1

SECTION 1

INTRODUCTION

BACKGROUND

A new non visual precision approach and landing guidance system has been accepted by the International Civil Aviation Organization (ICAO)¹ as the future international standard.

The federal Aviation Administration (FAA) proposed Microwave Landing System (MLS), is based on the Time Reference Scanning Beam (TRSB) technique in which time between successive scans of narrow fan beams provide elevation and azimuth information to aircraft within a designated service volume. Distance information is provided by existing Distance Measurement Equipment (DME) or by new Precision Distance Measurement Equipment (PDME), both operating in L-band (960 to 1215 MHz). Current proposals call for channel pairing between these L and C-band guidance functions. APPENDIX B contains a system description of the MLS angleguidance and range-guidance equipments.

Early in the development of the MLS, the Electromagnetic Compatibility Analysis Center (ECAC) developed an automated channel assignment model that was capable of performing intersite analyses and making channel assignments for the MLS functions as they were envisioned in 1972². Subsequent refinements to the MLS system design and implementation plans have resulted in a requirement for a more complex channel-assignment model.

Time Reference Scanning Beam Microwave Landing System, DOT/FAA, December 1975.

²Frazier, R., In-Band Compatibility Analysis of the RTCA-Proposed Microwave Landing Guidance System (LGS) and Interim System, (FAA-RD-75-62), ECAC, Annapolis, MD., July 1972.

^aChannel pairing is when frequency assignments in different bands are interdependent. This enables a pilot to automatically use equipments of different bands by tuning to a single channel.

One of the major changes is that the PDME function has been moved from C-band (5.0-5.25 GHz) to L-band (960 to 1215 MHz). The current plan calls for possible assignment of the PDME function to existing L-band X and Y mode channels used by conventional DME systems. Additional L-band channels are expected to be created by defining new operating modes (i.e., multiplexing) on the present L-band frequency pairings.

The L-band TACAN/DME X and Y mode channels are currently channel paired to VHF (ILS Localizer and VOR) and UHF (ILS Glideslope) channels. Dependent upon the final implementation strategy, assigning the PDME functions to these L-band channels may result in channel-pairing of aeronautical radionavigation equipments in four bands: MLS angle-guidance equipment in C-band; TACAN, conventional DME and PDME equipments in L-band; ILS Localizer and VOR equipments in the VHF band; and ILS Glideslope equipments in the UHF band. Coupling between bands could therefore result in a need, when making MLS assignments, to check MLS C-band angle-guidance assignment criteria with potential assignment criteria in the L, VHF, and UHF bands.

In addition, the model reflects the FAA requirement that greater accuracy be provided in predicting the value and location point within the MLS protected service volume of the minimum desired-to-undesired signal power ratio (D/U).

OBJECTIVES

The objectives of this effort were to develop an automated channel-assignment model capable of providing frequency assignments of MLS equipments that operate either in C-band or L-band, and to provide a trial channel assignment predicated on a specific test environment and channelization scheme that utilizes existing VHF and UHF channels.

APPROACH

In developing an automated channel-assignment model (CAM), it was necessary that the CAM be capable of providing MLS frequency assignments that would allow operation on a non-interference basis of the new MLS equipments with the present

airport and enroute equipments³. These combined environments include MLS angle-guidance equipment to be assigned to C-band channels; DME, PDME and TACAN range-guidance equipment in L-band; ILS localizer and VOR equipment in the VHF band; and ILS glideslope equipment in the UHF band.

To satisfy the need for an intersite analysis, as well as to provide channel assignments, two routines were developed. The intersite analysis routine was designed to calculate the minimum desired-to-undesired signal power ratio (D/U) within a desired facility's service volume. This analysis can be performed for either/or the sector/circular service volumes associated with ILS and MLS as well as the sector/circular service volumes of TACAN/DME and associated VOR equipments. The D/U ratios are calculated using equipment location and equipment characteristics obtained from the user-specified airport environment. Propagation loss predictions are provided by a model developed for the FAA by the Institute for telecommunications Sciences (ITS). The intersite analysis results consist of predicted minimum D/U ratios for each equipment pair within the same frequency band.

The channel-assignment routine was designed to use the D/U values from the intersite analysis and convert them into minimum channel-separation requirements based on user-specified D/U protection criteria. Using these separation requirements and the frequency resources contained in a user-specified channel plan, a denied-channel array is generated. This array indicates those frequencies that are not available for use by each equipment to be assigned. If the user chooses the dynamic approach, a scan of the array determines the most constrained equipment, in terms of the remaining frequency resources available for its assignment.

Analysis of MLS Channel Plans with L-Band DME, Inter-Agency Agreement, DOT-FA76WAI-6]2, Task Assignment.

⁴Gierhart, G.D. and Johnson, M.E., Propagation and Interference Analysis Computer Programs (0.1 to 20 GHz), Applications Guide, FAA-RD-77-60, ITS, Boulder, Colorado, March 1978.

The most constrained equipment is that which has the minimum number of available frequency resources. This equipment is assigned first. The denied-channel array is subsequently updated to include new constraints imposed by the channel just assigned, and the process is then repeated until all equipments are assigned or channel resources have been exhausted.

The channel-assignment model can assign equipments in each of the four bands (UHF, VHF, L-band, and C-band) and can make assignments for channel-paired equipments. Dependent upon user specified operating conditions it is also capable of reassigning existing preassigned equipment if their present operating frequencies cannot satisfy the channel-separation requirements of the new channel paired MLS functions.

In addition to the development of the intersite analysis routine and the channel-assignment routine, it was necessary to identify the types of data required to support those routines during their use. These data are documented as part of the assignment system.

A trial assignment was made to appraise the assignment model's performance in a working environment, as well as the performance of an FAA-proposed equipment channelization scheme.

The environment used to test the assignment model was an updated Southwest U.S. airport environment that had been developed by the FAA in support of the Radio Technical Commission for Aeronautics Special Committee 117 (RTCA in 1972). This environment included a four-state area and is listed in APPENDIX D.

The differences between the 1972 environment and the present version are:
1) addition of MLS-PDME requirements to L-band; 2) addition of existing preassigned

a"Preassigned" refers to existing ILS/VOR or TACAN/DME equipments operating on a designated channel. When the new MLS and PDME systems are frequency paired to these existing equipments, their frequencies are predetermined in that the only MLS channel available for assignment is that which is hard-paired to the existing frequency assignment.

TACAN/DME and VOR enroute facilities, and existing preassigned ILS Localizer and Glideslope airport facilities to the UHF VHF-bands; and 3) addition of "dummy" equipments for the optional protection of paired frequencies where no associated equipments are physically installed.

The assignment was made using the channelization plan listed in APPENDIX

E. The list of frequency resources that was used in this first trial channel assignment was derived by pairing the C-band Frequency Channel Plan with the L-band PDME Interim Channel Plan. The assumptions used to derive the specific list of frequencies and to define the potential interdependence between the C-, L-, VHF and UHF bands are as follows:

- 1. C-band channels used for MLS angle-guidance were hard-paired to specific L-band channels. For example, C-band channel 002 (5031.6 MHz) was paired with L-band channel 18X (979 MHz). If either one of these channels was assigned to a facility, both of them were protected. If both could not be protected during the assignment process, neither could be assigned to that facility. This is repesentative of intrasystem hard pairing.
- 2. The existing channel-pairing required by ICAO Annex 10 between certain L-band channels, VHF channels, and UHF channels became part of the MLS channel plan. For example, channel 18X now pairs C-band (5031.6 MHz) with L-band (979 MHz), VHF-band ILS Localizer (109.10 MHz) and UHF-band ILS Glideslope (334.7 MHz) frequencies. As in (1) above, the assignment of any one of these frequencies at a facility requires the protection of all related hard paired frequencies, even though some of the equipment was not actually required. This is representative of intersystem hard pairing.

The protection criteria used in this first trial assignment is presented in APPENDIX C. Included in this appendix are some qualifying statements, and a listing of the criteria for all four frequency bands, i.e., C-band, L-band, and the VHF and UHF bands. It should be noted that consistent with traditional FAA procedure, only ground-to-air L-band interference interactions were considered.

SMLS Signal Format and System Level Functional Requirements, FAA-ER-700-08C, 10 May 1979.

FAA-RD-80-91

Section 2

SECTION 2

MODEL DESCRIPTION

INTRODUCTION

The MLS channel-assignment system was designed to provide MLS frequency assignments compatible with existing airport and enroute environments. The system was constructed in three parts, an intersite analysis, a channel-assignment model, and a supporting data base. The overall program flow is illustrated in FIGURE 1.

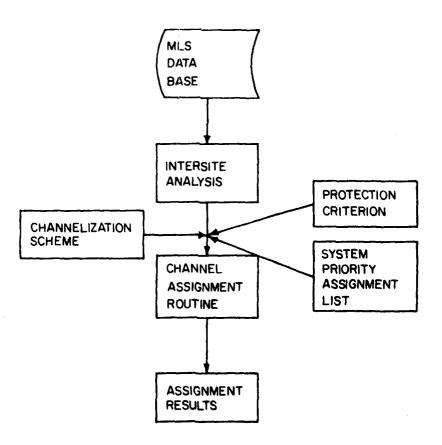


FIGURE 1. MLS CHANNEL ASSIGNMENT SYSTEM.

The system was designed so that the intersite routine and channel-assignment routine can be run independently. The results of the intersite analysis can be stored and reused for each assignment routine run. Hence it is generally not necessary to rerun the intersite analysis for each channel-assignment attempt.

A measure of the models usefullness during the MLS equipment development is its ability to accommodate various channelization schemes and assignment conditions that a user may wish to investigate. The flexibility to use varied schemes and conditions is accomplished through manipulating the model inputs (MLS data base, equipment protection criteria, channelization scheme, and equipment priority list) as well as selecting the use of several preprogrammed assignment options that control the internal assignment process. A discussion of the options and capabilities of the model that are available to the user is included in Section 3.

INTERSITE ANALYSIS

The intersite analysis routine examines the interference potential between two equipments and determines the minimum, i.e., worst-case, desired-to-undesired signal power ratio (D/U) at a receiver within the protected service volume of either equipment. The analysis is performed between equipments operating in the same frequency band.

The analysis has two parts, a distance culling procedure to identify those equipment pairs whose separation distance precludes interference, and a method for calculating the minimum D/U for the remaining equipment pairs. The intersite analysis program logic flow is shown in FIGURE 2.

Distance Cull

For each equipment pair, the model establishes two boundaries, a small circle defined by the victim service volume radius, and a larger circle representing the minimum distance separation for safe cochannel operation for the

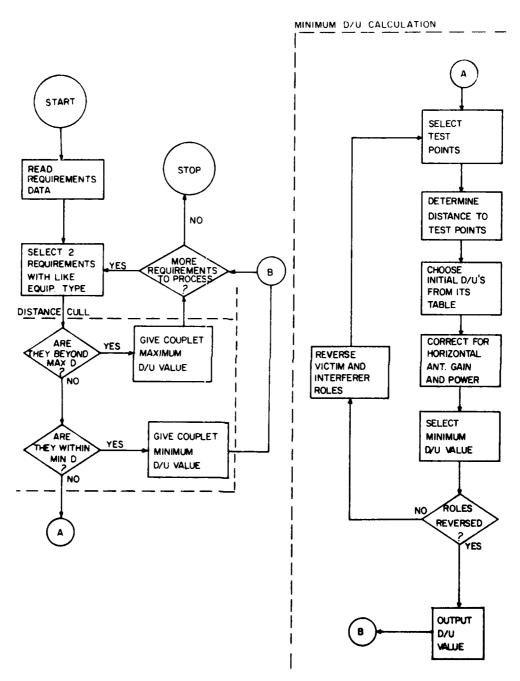


FIGURE 2. INTERSITE LOGIC FLOW.

two equipments (see FIGURE 3). An equipment pair separated by more than the cochannel distance boundary is assigned a cochannel D/U value. An equipment pair separated by less than the service volume distance boundary is assigned a worst-case D/U value, as defined by the protection criteria. The balance of the equipment pairs will require further analysis to determine the minimum D/U value, as shown in area B of FIGURE 3.

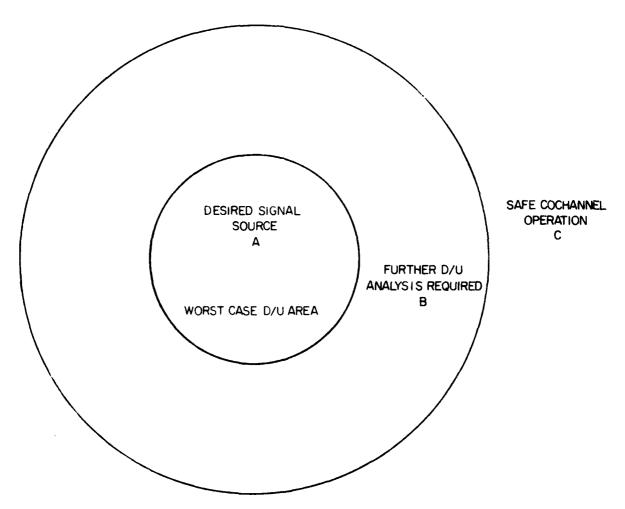


FIGURE 3. DISTANCE CULL BOUNDARIES

Minimum D/U Calculation

The minimum D/U is determined by calculating D/U ratios at critical test points (receiver locations) in the desired signal service volume and selecting the smallest value. The model is designed to analyze the circular service volumes associated with TACAN, VOR, conventional DME, and PDME equipments, as well as the various sector/circular service volumes associated with the ILS (Localizer and Glideslope) and MLS equipments. The location of the test points to be used was determined by an analysis described in APPENDIX A. In this analysis, it was shown that the minimum D/U value within the tailored service volumes associated with MLS and ILS equipment will occur at the maximum service volume range near one of three points. Those points, shown in FIGURE 4, are the corner points (B and D), and the intersection of the line connecting the desired and undesired equipments and the boundary of the desired equipments service volume, point (C).

The closest point may not have meaning when the non-circular tailored service volumes are used in the analysis. In a tailored service volume, if the undesired source is located within the angular limits of the desired service volume (case #1 in FIGURE 4), three points are selected, one at each corner of the service volume, and a third at the line connecting the desired and undesired source. When the undesired source is outside these angular limits, only the corner points are tested (case #2 in FIGURE 4). For circular service volumes, the angular limits are always considered to be $\frac{1}{2}$ 180°, making the undesired source always fall within the angular limits of the desired service volume. For that case, the model always uses the point on the line connecting the equipments, at the maximum service range.

The D/U calculation at each critical test point is performed by considering both the azimuth and elevation of the test point location with respect to the desired and undesired signal sources. A propagation model developed by ITS (Reference 4), which is based on a 95% time availability basis, has been integrated into this intersite analysis to calculate an initial D/U value for each test point based on the desired and undesired signal propagation losses and their vertical antenna gains in the direction of the victim receiver. These initial

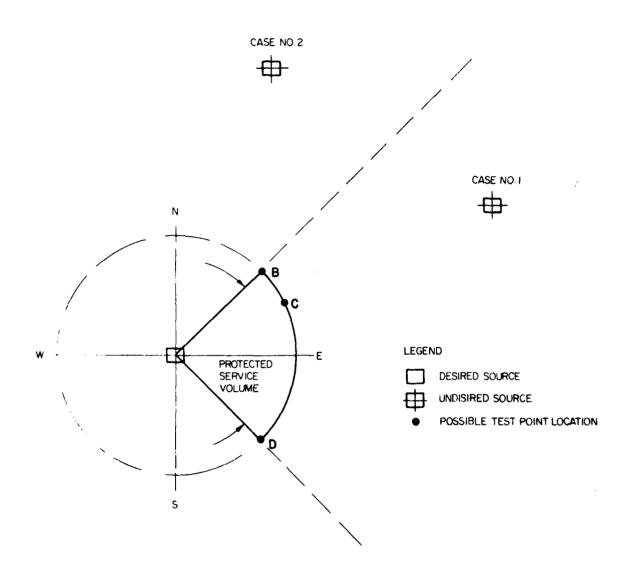


FIGURE 4. TEST POINT LOCATIONS IN A SECTOR SERVICE VOLUME.

 $\rm D/U$ values are stored in a series of look-up tables prepared for each type of equipment. To obtain the final D/U values the initial D/U's are adjusted for transmitter power and horizontal antenna gain differences. The minimum D/U ratio is selected from this set of values.

The initial D/U ratio at each test point is determined by calculating the desired-to-undesired ground equipment separation distance^a, and interpolating from tabulated D/U curves prepared in advance. Every equipment service volume configuration (e.g., MLS, 20 nmi, and DME, 25 nmi, etc.) has a tabulated D/U curve to be used when that equipment undergoes analysis. FIGURE 5 shows the $D_{\rm F}U$ curve prepared for an MLS 20 nmi service volume. Each curve has been constructed so that the D/U value at each site separation distance is the minimum that will occur at any altitude within the service volume limits.

The initial D/U values determined using the ITS curves are then adjusted by incorporating the difference between the desired and undesired signals, horizontal antenna gain in the direction of each test point, and the difference in transmitted power values between the desired and undesired signal sources, with the initial tabular D/U value.

The final D/U values calculated at the critical test points within the service volume of the desired source are then compared and the minimum D/U is stored. At this point, the model reverses the roles of the two equipments for the couplet being analyzed. The desired signal becomes the undesired signal and vice versa. The analysis is repeated using the same procedure described above, to calculate a second minimum D/U value. This second value is compared to the first value and the final minimum D/U is stored for use in the channel-assignment routine. The result is the smallest D/U value in the service volume of either equipment and its use assures the protection of both equipments.

The intersite analysis is performed for each individual equipment in an environment, with every other equipment in the same frequency band. At an

a Equipment separation distance is the combination of the desired equipment-to-test point plus undesired equipment-to-test point distances.

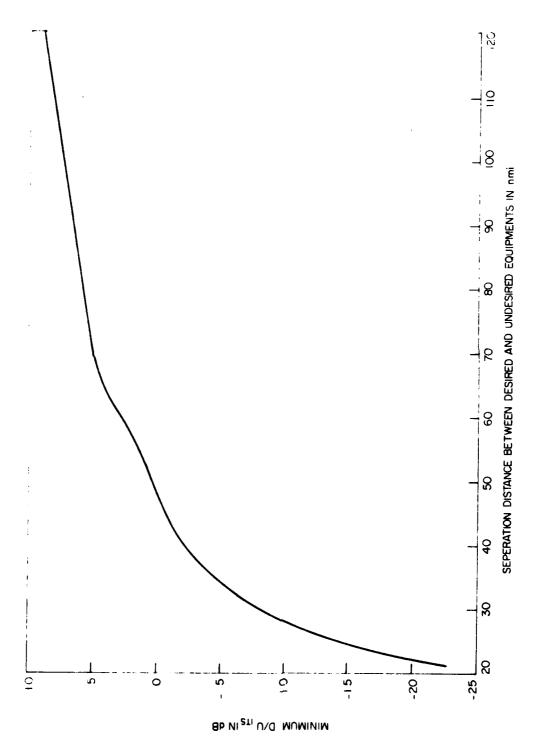


FIGURE 5. COMPOSITE D/U $_{\mbox{\scriptsize ITS}}$ CURVES FOR 5,000, 10,000 and 20,000 FEET ALTITUDE.

airport facility where several different equipments are operating and providing various services, there will be a set of minimum D/U values, one associated with each of the equipments.

CHANNEL ASSIGNMENT

The channel-assignment model examines the intersite constraints existing between the equipments in a working environment, and assigns channels providing the channel separation required by the protection criteria. The user specifies the inputs to the routine: 1) the channelization scheme; 2) the protection criteria; 3) the data base defining the equipment operational parameters; and 4) the method of determining the priority of equipment assignments.

In addition to specifying the above inputs the user may also select preprogrammed options: 1) alternate channel pairing schemes; 2) reassignment of existing equipment assignments to other channels, and; 3) a display of the percentage of channels denied to equipments that fail to be assigned. A description of the model options and capabilities is included in section 3.

The assignment routine will be discussed in two parts, the denied channel array construction, and the final assignment process. The program flow is illustrated in FIGURE 6.

Denied Channel Array

The denied channel array is constructed prior to the beginning of the assignment process. It shows the frequencies that are available to each system^a of equipments and does not initially reflect any of the intersite constraints between systems. This array is constructed in two steps: 1) listing the frequency resources available to each equipment type; and 2) entering a frequency resource list for each equipment into an array, according to the hard-pairing between equipments.

^aA system is a set of equipments providing landing guidance at a runway site, or navigational guidance at an enroute facility. Each equipment in the environment to be assigned is identified with a system.

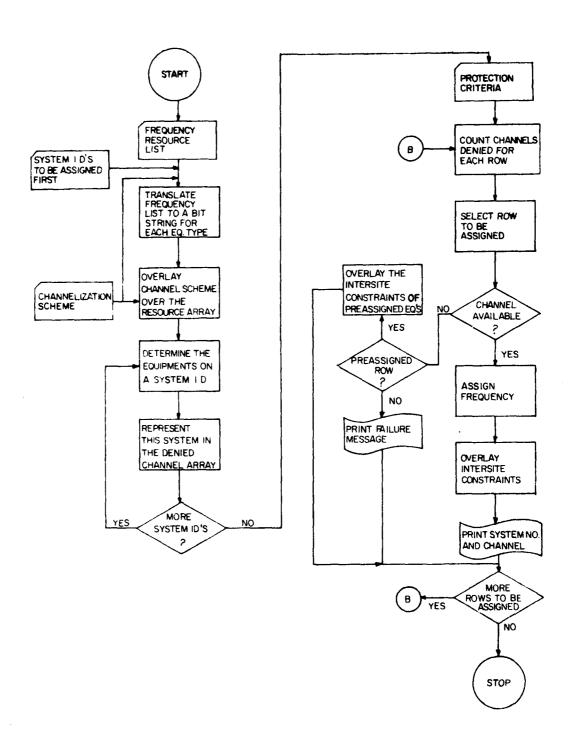


FIGURE 6. ASSIGNMENT ROUTINE LOGIC FLOW.

The first step is the creation of a frequency resource list for each equipment type to be considered in the assignment process. The channelization scheme defining the frequency resources available to each type of equipment is converted to a bit string, with "O's" indicating the available frequencies and "l's" indicating the denied frequencies. Step 1 of FIGURE 7 illustrates a frequency resource list constructed from the partial channel scheme listed.

The second step is to construct a denied channel array with columns representing frequency resources and rows representing the equipments to be assigned. Frequency resource lists for all equipments in a system are entered into the array according to equipment type and the required hard-pairing between equipments within each system. The model identifies the hard-paired equipments within a system and overlays their resource lists. Any frequency resource that is denied for one of the equipments results in the elimination of the corresponding resources on that channel for the entire hard-paired set. The result is an array showing the frequency resources available to each system of equipments.

Step 2 of FIGURE 7 illustrates the denied channel array row representing a hard-paired system of equipments composed of MLS, DME, ILS, and Glideslope. Four channels are available to their system: 18X, 18Y, 20X, and 20Y. In the event that no hard-pairing between equipments is desired, the denied channel array of FIGURE 7 would contain the four individual resource lists corresponding to the equipments that are listed, and no overlaying of these lists would occur.

When a system is preassigned (i.e., it is an existing system in the environment operating on a specific frequency), all channels except the preassigned one are denied to it. For example, if the system of FIGURE 7 were preassigned on channel 18X, all other channels would contain "1's" in the denied channel array shown. The user also has the optional capability to ignore the preassigned channel so that the system will be allowed assignment on any channel. Conversely, any system can be proposed for assignment on a specific channel by specifying for it a preassigned channel when the array is constructed.

Channel	MLS Angle	PDME	DME	VOR	ILS	Glideslope
17X			978	108.00		
17Y	5031.0	1,104	1,104	108.05		
17XC	5031.3	978				
18X	5031.6	979	979		108.10	334.70
181	5031.9	1,105	1,105		108.15	334.55
18XZ	5032.2	979	1			
19X			980	108.20		ì
19Y	5032.5	1,106	1,106	108.25		
1982	5032.8	980	ļ			
20X	5033.1	981	981		108.30	334.10
207	5033.4	1,107	1,107	li	108.35	333.95
20XI	5033.7	981			<u> </u>	

Step 1

Frequency Resource List

	17	18	19	20
	X Y XZ	X Y XZ	X Y XZ	X Y XZ
MLS Angle	100	000	100	0 0 0
PDME	100	000	100	000
DME	0 0 1	001	0 0 1	001
VOR	001	111	001	111
ILS	111	001	111	0 0 1
Glideslope	111	0 0 1	1 1 1	001

Step 2

Denied Channel Array

	17	18	19	20
	X Y XZ	X Y XZ	X Y XZ	X Y XZ
MLS Angle DME ILS Glideslope	1 1 1	0 0 1	1 1 1	001

0 - channel available

1 - channel not available

FIGURE 7. DENIED CHANNEL ARRAY CONSTRUCTION.

Assignment

The assignment model uses the denied channel array to systematically assign each system in the environment to an available channel. After each successful assignment, the denied channel array is updated to reflect the intersite constraints between the most recently assigned system and all the remaining unassigned systems. The minimum D/U values between each system, calculated in the intersite analysis, have been translated into the channel separation required for safe operation as defined by the protection criteria listed in APPENDIX C. These channel separations determine the channel spacing required between systems when updating the denied channel array.

In normal operation, the model begins assigning systems by counting the frequency resources denied to each system (row) and first assigning those systems with the fewest remaining resources. As an option, the model may select the first system to be assigned from a list specified by the user. The row representing this first system to be assigned is searched for an available channel, and the first free channel is assigned. If no channel is available, the model prints a failure message and proceeds to the next assignment.

When an assignment is made, intersite constraints may be placed on some of the remaining unassigned systems. If necessary, the channel assigned, and some number of adjacent channels will be eliminated from the rows of potentially interfering systems. This process updates the denied channel array for the next assignment attempt.

FIGURE 8 illustraces the channel assignent process for three systems, beginning with the denied channel array. System one is assigned its first available channel, and the denied channel array is updated to reflect the channel separation required between the systems, as a result of this assignment. The process continues in the same manner, until assignment has been attempted for all systems.

^aThe sequence of channels as listed by the user represents an optional capability.

	В	egin - Denie	ed Channel	Array	
	17	18	19	20	
System	X Y XZ	X Y XZ	X Y XZ	X Y XZ	Protection Required
l.MLS Angle DME ILS Glideslope	1 1 1	0 0 1	1 1 1	0 0 1	l→2 Channel l→3 channel 2→3 2 channel
2. MLS Angle DME HLS	111	0 0 1	1 1 1	0 0 1	Assign System 1 Channel 18 X
3. MLS Angle PDME	100	0 0 0	1 0 0	0 0 0	
	15	ST - Updated	l Channel Ai	rray	
	17	18	19	20	
System	X Y XZ	X Y XZ	X Y XZ	X Y XZ	
2	1 1 1	1 0 1	1 1 1	0 0 1	Assign System 2 Channel 18 Y
5	100	1 0 0	1 0 0	0 0 0	Chamer 10 at
	2.5	ID - Updated	Channel Ai	ray	
	17	18	19	20	
System	X Y XZ	X Y X2	X Y XZ	X Y XZ	
5	100	1 1 1	100	000	7 Available Channels for Assignment

FIGURE 8. CHANNEL-ASSIGNMENT PROCESS.

It should be noted that for clarity purposes in this example, channels 17X, 17Y and 17XZ have been treated simplistically as adjacent channels. However, in reality this is dependent upon the channel plan definition. An examination of the channel plan defined in APPENDIX E reveals that the C-band frequencies contained in channels 17X, 17Y and 17XZ are adjacent frequencies, but that the L-band frequencies are not. L-band channels 17X and 18X contain adjacent frequencies. Therefore, when the denied channel array is updated by the channel assignment system to reflect the impact of a particular assignment on adjacent channels, each band is updated separately, and the results are combined (logical OR) to decide if a particular channel (paired set of frequencies) is available for future use.

Additional note should be made of the effect of using the APPENDIX E channel plan. Adjacent channel restrictions would usually affect separate L- and C-band channels, thus in some cases denying twice as many channel numbers as may be required for a more optimally defined plan.

A special situation arises when assigning systems containing preassigned equipments. In the assignment process, an existing preassigned system, hard-paired with a new MLS equipment, may be unable to use its existing "preassigned" channel because of intersite constraints placed on the MLS from prior assignments. In this case, a reassignment option is available to the user, and allows the assignment routine to search for any available channel to assign the entire system; planned plus existing. If this option fails, the hard-pairing requirement may be relaxed at the discretion of the user, thus allowing the planned MLS portion to be assigned separately from the existing equipment.

DATA BASE

The MLS data base consists of an individual data record for each equipment in the environment. Each equipment (subsystem) record contains a system identification number which links it with other equipments that form a system at the

same facility in the environment. A system is a set of equipments providing landing guidance at an airport, or navigational guidance at an enroute guidance site. An airport facility may contain many systems, associated with various runways.

A data record contains information for both the equipment, and the airport/enroute facility where its associated system is located. The equipment information includes the type and location, as well as the service and operational parameters. The facility information includes the identification, location, and service capability of the airport or enroute site.

A user wishing to create a new environment for use in the channel assignment model must provide the information needed to construct a data record for each individual equipment in that environment. Certain of the information contained on the data record is not crucial to the actual operation of the assignment model. The information that is necessary for the model operation and must be supplied, is identified by an asterisk in the description that follows. The information contained on each equipment record is as follows:

Equipment Dataa

- 1. Equipment Type* Identifies the type of equipment contained on the record (e.g., TACAN, VOR, etc.).
- 2. Equipment Lat./Long.* (degrees, minutes, seconds) Latitutde and longitude of the equipment location.
- 3. Channel* The designated channel of a preassigned L-band or VHF equipment.

^aAPPENDIX B defines equipment parameters and service options for each equipment type.

4. Frequency $(MHz)^*$ - The operating frequency of a preassigned L-band or VHF equipment.

- 5. Service Radius* (nmi) The radius of the protected service volume.
- 6. Altitude (ft.)* The maximum protected altitude within the service volume.
- 7. Service Volume* Type of L-band or C-band service volume coverage (e.g., High, Low, Terminal, MLS Service Volume). This parameter should be specified when the service volume is of a standard type. The standard service volumes in use are listed in APPENDIX B.
- 8. Option* Type of ILS service coverage. (Standard, Option 1, Option 2, Option 3). This parameter should be specified when a standard option, listed in APPENDIX B, is chosen.
 - 9. Gain (dBi)* Mainbeam antenna gain.
 - 10. Power (kW)* Effective power input to the antenna.
 - 11. Antenna Pattern* Type of vertical antenna pattern.
 - 12. Height (ft.)* Transmitter antenna height.

Facility Data

- 1. Airport/Enroute Facility Number* This is the system identification number; it identifies the system, or group of equipments, providing guidance to a specific runway or enroute navigation site (i.e., all equipments associated with a runway/enroute site have the same facility number). Each equipment data record must have a facility number to insure that the equipments to be channel-paired at each site can be identified.
- 2. Location* The city and state of an airport facility, or the state and location of an enroute site.
- 3. Airport Lat./Long. (degrees, minutes, seconds) The latitude and longitude of airports (no entry for enroute facilities).
- 4. Bearing of Runway (degrees)* The bearing of a runway associated with an airport facility.
- 5. Facility Call Number Three alphanumeric characters identifying an airport facility or enroute site.

6. Airport Type - Categories designating the status and type of service for an airport facility.

New - not in existence

General Aviation - general air traffic

Air Carrier - all commercial aviation

V/STOL - special takeoff and landing facility

- 7. Tower Exist Indicates whether a tower exists.
- 8. Runway Exist Indicates whether a runway is in existence.
- 9. Frazier's Number The number assigned to a system in the proposed environment developed in 1972.
- 10. Link Number* A link number identifies those equipments which must operate on the same frequency. This situation arises when two like equipments are located at opposite ends of a runway, or on adjacent parallel runways, but do not operate simultaneously. By linking equipments, all guidance for a runway will be on the same frequency.
 - 11. Runway length (ft.)
 - 12. Runway Width (ft.)

Section 3

FAA-RD-80-91

SECTION 3

USER OPTIONS AND MODEL CAPABILITIES

GENERAL

The MLS Channel Assignment Model was constructed principally as a tool for evaluating the various channelization schemes proposed for the MLS angle guidance and range guidance equipments. In order for the model to handle a variety of channel plans, perhaps requiring special environmental assignment considerations, it was necessary to provide certain options that give the user sufficient flexibility to test particular ideas. User options are accomplished in two ways: (1) through the main inputs to the model and (2) by selecting internal system options that regulate the assignment process. By utilizing these options, the user may investigate assignment ideas in different airport environments, using various MLS characteristics and with specialized protection criteria. This section will describe these options and some example problems that can be investigated using this assignment model. The current use of this channel assignment model at ECAC is accomplished through the FAA Spectrum Support Office.

USER OPTIONS

The following is a description of the input options and model options available to the user.

Input Options

The main input options under user control are the equipment protection criteria, the channel plan, the data base including the environment description, and the assignment priority list. By controlling these key inputs, many options are available to the user.

<u>Protection Criteria</u>. The protection criteria places upper bounds on the undesired signal level (U) with respect to the desired signal level (D) that provide for interference-free operation of the potential victim equipment

within standard protected service volumes. Levels are specified as a D/U power ratio for cochannel and adjacent channel undesired signals. Different criteria are used in each frequency band as described in detail in APPENDIX C. The user has the option of specifying established protection criteria or updated criteria based on analytical or emphirical results as equipment designs change.

The L-band protection criteria included in TABLE C-1 are consistent with current FAA frequency assignment methods found in the U.S. National Standard for the VORTAC System for X-mode channels. However, the planned use of multiple-modes for the MLS range guidance system and the planned revision of the national standard to consider the source/type of the undesired signal, have spawned the need for a more detailed specification of L-band protection criteria. In particular, the L-band protection matrix shown in TABLE 1 satisfies the structure needed to specify the required criteria. This matrix treats each combination of victim equipment and potentially interfering equipment on an individual basis, allowing the interference rejection advantage of the newer PDME equipments to be reflected in the assignment process. The user simply needs to provide the applicable inputs. As the MLS range guidance system matures or as older conventional TACAN/DME systems are deleted from the operational inventory, these criteria can be updated at the option of the user.

The C-band protection criteria included in TABLE C-2 were based on analytical work by ECAC and the Bendix Corporation, and substantiated by emphirical testing at NAFEC. As with range guidance protection, these criteria are under user control and may be updated as the system matures.

The VHF and UHF protection criteria are contained in TABLES C-3 and C-4 respectively for the VOR, ILS Localizer and ILS Glideslope systems which are channel-paired to selected L-band frequencies as outlined in Section 1. The thresholds are planned for incorporation by the FAA into the revised national standard. Again, as with L- and C-bands, these criteria are under user control and can be updated as required.

TABLE 1

SAMPLE L-BAND PROTECTION MATRIX IN dB

Undesired Source	 	TACAN		MO	DME (100W)			PDME	
Desired Source	TACAN	DME	POME	TACAN	DME	PDME	TACAN	DME	PDME
Cofrequency, Co-aperture	8+	8+	8+	+8	89+	8+	8+	8+	+8
Cofrequency Out-of-aperture			-50			-50	8 +	+3	-50
First adjacent frequency, Co-aperture	-42	-46	09-	-29 ^a	-29ª	09-	-75	-25	09-
First adjacent frequency, Out-of-aperture			-75			-75	-34	-34	-75
Second adjacent frequency, Co-aperture	-50	-54	-75	-38	-38	-75	-34	-34	-75
Second adjacent frequency, Out-of-aperture			-75	1		-75	-34	-34	-75

^aFor an undesired IKW DME, these D/U become -39dB

 $^{
m b}$ If PDME systems are assigned on conventional X or Y channels, the required protection criteria is the same as for conventional TACAN/DME equipment.

Channel Plan. The channelization scheme defines the frequencies that are available in each frequency band and identifies each set by a channel number. The MLS Channel Assignment System is capable of accepting channel plans with paired frequencies from four different bands for each channel number. A proposed channel plan is listed in APPENDIX E. Note that the L-band frequencies are in two sets, those available for conventional TACAN/DME equipment and those available for PDME equipment.

A channel plan may contain any number of channels with any subset of frequencies from the C-, L-, VHF-, and UHF-bands defined for each channel. The assignment model will accept any number of modes (pulse-pair spacings) within the L-band portion of the channel plan, and the channels may be listed in any order desired. TABLE 2 shows a sample channel plan containing 10 channels, each with paired frequencies from more than one band. Note some options available to the user in defining channels in the sample plan. Channel 18X contains frequencies from all four bands and allows MLS angle and range guidance, conventional TACAN/DME, and a complete IIS system to operate on that channel. However, channel 18B is an exclusive MLS channel for angle and range guidance only, and channel 19X is not available for MLS use but only for enroute VOR-DME facilities.

TABLE 3 shows this same plan with the channels listed in a different order. This ordering option gives the user the choice of defining a particular channel implementation sequence or "packing order". This determines the order in which the assignment model will search for an available channel during the dynamic assignment process. For a channel plan as listed in TABLE 3, the assignment model will search for an available channel starting with 18X for each assignment attempt and continue searching through 19X, 18Y, 19Y, etc., until an available channel is found or until the channel resources are exhausted. In this manner, successful facility channel assignments are "packed" on the left-most channels, thus saving those on the right for later implementation.

Data Base. The MLS Data Base contains the equipment operational parameter and facility information required by the assignment model when performing an assign-

TABLE 2

EXAMPLE CHANNEL PLAN

5031.60 5031.9 5032.2 5032.5 979.0 1105.0 108.1 108.15	18A 18B 18C	18C 19X 19Y.	19Y .	19A	198	190
979.0 1105.0 979.0 979.0 979.0 979.0 979.0 979.0 1108.1	5032.5	8.	5033.1	5033.4		5034.0
979.0 1105.0 108.1 108.15	0.626		1106.0	980.0	0.086	980.0
108.1 108.15	;	0.086	1106.0	1	1	;
	:	108.2	108.2	;	1	;
	;	;	1	;	1	;

TABLE 3

ALTERNATE PACKING ORDER

											-
	18X	X61	18Y	197	18A	18A 19A	18B	198	18C	190	
MLS	5031.6	 		i	5032.2	5033.4	5032.5	5033.7	5032.8	5034.0	
POME	979.0	:	1105.0	1106.0	979.0	0.086	979.0	0.086	979.0	0.086	
TACAN/DME	979.0	980.0	1105.0	1106.0	ţ	{	:	!	:	:	
ILS/VOR	108.1	108.2	108.15	108.25	1	;	;	1	:	ł	
Glidescope	334.7	ł	334.55	;	1	i	:	:	f	;	
											_

ment. Section 2 contains a listing of the information contained in the data base. This information is initially entered on data cards after which it is processed and organized onto record files containing all the required equipment data at a specific runway. FIGURE 9 shows the resulting compiled records for four ways in the Northeast United States.

Currently, there are three environments contained on MLS data base records. The first is a Soutwest United States environment containing the existing and planned airport and enroute equipments in a four-state soutwest region, including the Los Angeles basin. This environment was based on a predicted 1980 airport environment which included proposed new facilities as they were envisioned in 1972. A listing of this environment is contained in APPENDIX D. The second environment is a modification of the first made by deleting many of the proposed runways which were not built by 1980. The third environment consists of 20 states in the Northeast, East Central and Southeast United States region. All of these environments include high density airport regions that present conservative conditions from a channel assignment standpoint.

The MLS data base structure was intended to provide flexibility to the assignment model in that the key information needed for an assignment is contained in the data base record, which can be easily changed to suit a user's wishes. Equipment records can easily be added to or deleted from the data base through preprogrammed maintenance routines. In addition, records can be altered on an individual or environment-wide scale. This gives the user the capability of altering, for instance, the service volume coverage, transmitted power, antenna gain and radiation patterns of individual equipment records, or a specific type of equipment throughout the entire environment.

Equipment Assignment Priority. The normal operation of the channel assignment model uses a dynamic ordering technique to determine the order in which equipment will be assigned channels.

FACILITY LOC NUMBER STAT	LOCATION STATE/CITY	FACILITY Latitude Lombitude	ITY LOMGITUDE	REAR FAC	FAC	A LAPORT T	TYPE	TOWER R	RUMBAY F Exist	FR42IER NUMBER	LINK	FUAMAY LENGTH	PUNHAV W TO TH	AGENCY	
1 CT/BRID6EPO	D&EPORT +1	N 60 60	073 07 35 W	330	808	EXS ATR C	CARD	9	YES	C	-	4677	150	F A 4	
EQUIPMENT SMALL COMNTY ILS-OME P-OME ILS 1 GLIDESLOPE-1	LATETUDE #11 09 958 N #11 09 30 N #11 09 55 N	CONSITU 273 07 273 07 073 07 073 07	CHARME 212 M 90 X 22 M 90 X 32 M 90	FFF 0 1005.000 111.700 350.200	20 20 20 20 20 20 20 20 20 20 20 20 20 2	ALT SERVICE 2000 MLS 12000 PERMIN 2000 TERMIN 4500		23.0 23.0 11.0 11.0 11.0 11.0 11.0 11.0 11.0 1	POWER 1.8 100.0 100.0	PAT SM.CM. CARDIO PDME WILCOX NUCL	- 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	101 091 081 150 8	19 0	(-)v	# o d o o o
FACILITY LOC NUMBER STAT	LOCATION	FACILITY LATITUDE LON	LONGITUDE	1.3 8 4.3 F	Ar.	1 1400414	146	EXIST F	PUMBAY	FRAZIER Number	LIVE	FUNBAY	AUNE N H IDTH	40 c 4C Y	
, CT/841	CT/BRIDGEPONT 41	09 49 N D73	N 25 TO 575	162	# O #	EXS AIR CAR	ů æ	0	YES	o	-	4677	15.0	٠,٠	
EGUIPHENT SMALL COMMITY MANKER BECOM PANKER BECOM	LATITUDE #1 09 #9 K #1 09 #9 K	LOW617U 073 07 073 07 073 07	DE CHANNEL 35 E 0 35 E 0	FRE 0 8 75 - 100 -		2	222	0PT GAIN 23.0 11.4	100 E	SM.CM. CARDIO PORE	+ 100 + 100	100 000	9HOR (+3 VE) 43 20-0 180 -0	100 C C C C C C C C C C C C C C C C C C	w in in in in
*115 \$ *15 \$	22	073 C7 073 C7 073 07		600		1000		2 5.0	-		, m.C.		~ ~	2	130
FACILITY LOC NUMBER STAT	LOCATION STATE/CITY	FACILITY LATITUDE LONGITUD	LONGITUDE	<u>.</u>		AIRPOOT TYPE	ابد	TOWER F	* +	FRÆZIER Number	LINK	RUNLAY LE VGTH	DUNKAY HIDIH	465NCY	
T CT/DANBURY	BURY *1	22 18 N	073 28 56 W) 18	a x o	EXS GENERAL	7	YES	YES	IJ	L)	0410	٠.٠	1 4 5	
EQUIPMENT SMALL COMNITY MARKER BECON P-TME	LATITUDE 41 22 18 N 41 22 18 N 41 22 18 N 41 22 18 N	LOM61TU 073 28 073 28 073 28 073 28 073 28	3 3 3 3 3 3 3 3 3 3 3 3 3 3 3 3 3 3 3	75. C00 75. C00 . C00 . C00 . C00	20 20 20 20 20 20 20 20 20 20 20 20 20 17 6 17 6 10 10 10 10 10	ALT SERVICE 2000 MLS 12000 TERMI 2000 TERMI 6250 TERMI	2 7 2	0PT GAIN 23.0 11.0 8.5 2.2 2 2.2 2 2 5.0	100 100 100 100 100 100 100 100 100 100	PAT SM.CM. CARGIO PDME COSINE WILCOX		1	## ## ## ## ## ## ## ## ## ## ## ## ##	Ĩ	granning Water
FACILITY LOCATION NUMBER STATE/CIT & CT/GROTON	LOCATION STATE/CITY //GROTON #1	FACI LATITUDE 19 47 N	LITY LONGITUDE 072 02 49 W	8 8 8 8 8 8 8 8 8 8 8 8 8 8 8 8 8 8 8	FAC CALL GON	AIRPOPT TYPE EXS GENERAL		EXIST EXIST	PUNEAY EXIST YES	FRAZIER Number J	LINK	90% BY LENGTH F300	9845UG #101# #151	46FNCY Far	
EQUIPMENT SMIL COMNTY ILS-DME PDME ILS-1 SLIDESLOPE-1	LATITUDE 41 2° 16 N 41 2° 16 N 41 2° 16 N 41 2° 16 N	LONGITUDE 072 02 14 072 02 14 072 02 14 072 02 14	CHANNEL IN E SOX IN E D IN E SOX	FREG .000 1011-C00 111-300 332-300	20 20 20 20 20 20 20 20 20 20 20 20 20 2	ALT SERVICE 2000 MLS 12000 TERMIN 2000 TERMIN 6250		0PT 6AIN 23.3 11.4 8.5 2 12.9 2 5.0	20 00 00 00 00 00 00 00 00 00 00 00 00 0	PAT SM.CM. CARDIO POME WILCOK	ក្នុង ខ្លួន ខេត្ត ខ្លួន ខេត្ត ខ្លួន ខេត្ត ខ្លួន ខេត្ត ខេត ខេត្ត ខ	100 (-1	(-)MOR (+) MY 20 183 35 35 35 35 35 283 283	# 5	271700 N#

FIGURE 9. DATA BASE RECORDS

This technique determines the equipment with the minimum number of available channels remaining in its list of channel resources, and attempts to assign that equipment next.

As an option, the assignment model is capable of accepting an assignment priority list specifying the order in which equipments will be assigned. Furthermore, the user may input an assignment order for only some of the equipments to be assigned; when this list is exhausted, the model will revert back to the dynamic technique for the remaining assignments.

The advantage of inputing a specific assignment order is that the user can simulate the actual order that equipment may be implemented. He may wish to place highest priority on the large metropolitan airports that require the newest equipment to meet their $n\epsilon$ eds, and lower priority on the smaller, less congested facilities.

Model Options

The main model options under user control are frequency pairing options, reassignment options involving preassigned ILS and DME equipment, and the option to display certain diagnostic information regarding the most likely cause of an assignment failure at a particular facility.

Pairing Options. The MLS channel assignment model has the capability of "hard pairing" equipment assignments in different frequency bands. Hard pairing requires that the guidance equipment associated with a specific runway must all operate on the same channel even though they may be in different frequency bands. This requirement makes channel selection at runway interdependent between the various equipments; if one equipment cannot be assigned on a given channel, the remaining paired equipments cannot be assigned. The following degrees of pairing are available as an option to the user:

1. total pairing of all the equipments at a runway site, i.e., hard pairing of equipments in all four bands.

2. no pairing between frequency bands, allowing all equipments to be assigned independently of equipments in other bands.

3. pairing of various combinations of equipments, for instance pairing of MLS C-band equipments with PDME at a runway site. Any combination of equipments can be paired in this manner.

Reassignment Option. Any existing or proposed airport environment developed to exercise the channel assignment model will contain a significant number of existing equipments (i.e., ILS) operating on preassigned channels. In the assignment process, these equipments are automatically assigned to their present operating channel. However, if new MLS or PDME equipments are hard paired to the existing equipment at the same runway, the existing preassigned channel may not provide the necessary interference protection for the new equipment in a congested environment. When this occurs, the entire hard-paired set of equipments will fail, including the existing preassigned equipment. The model declares that channel (i.e., hard-paired set of frequencies) to be not available at that site. The channel assignment system then provides two options to the user:

- 1. When a preassigned set of equipments fails to retain its existing channel, the entire set may be reassigned to any open channel, providing that channel contains a sufficient set of frequencies, or
- 2. Carrying the above option one step further, if the entire set of equipments at a particular runway cannot be placed on an open channel, the paired set of equipments can be broken and the proposed MLS and PDME equipments may be assigned to any open channel while the preassigned ILS Localizer and Glideslope will be placed each on their original channel.

Display the Most Constrained Equipment. When a paired set of equipments at a runway fails to be assigned a channel, it is desirable to know which equipment was most likely to have caused the failure. The channel assignment system has the capability of listing the percentage of the channels that are denied to each equipment in the paired set to show exactly which equipment

was the most constrained at the time of failure. This capability is intended as a diagnostic aid in determining those aspects of a channelization scheme that may be unworkable or most constraining.

SECTION 4

RESULTS

A channel-assignment model was constructed that is capable of performing an intersite analysis between interfering equipments in a user-input environment and assigning channels based on user designated intersite protection requirements and channelization scheme. A trial assignment was made for the Southwest U.S. airport environment listed in APPENDIX D.

The results of the first MLS trial assignment are summarized in TABLE 4. APPENDIX D contains a listing of the specific channels assigned to each system in the environment.

TABLE 4
TRIAL ASSIGNMENT SUMMARY

MLS Requiremen	ts	Successful	Assignments
Preassigned ^a	103	60	(58%)
New Assignments	252	237	(94%)
Total	355	297	(84%)

a"Preassigned" refers to new MLS systems which are frequency-paired to existing ILS-DME systems at the same runway. Therefore, their frequencies are predetermined.

It should be noted that in attempting to assign a C-band frequency to a "pre-assigned" MLS requirement, if the assignment failed for the existing channel, no alternatives were attempted (i.e., existing assignments were not changed in this first trial assignment).

The following is a summary of the most significant qualifications that should be used to place this initial trial in the proper context:

1. It was assumed that the PDME interrogator receiver would operate in the "narrowband" mode outside a radius of 5 nmi. This assumption resulted in an optimistic L-band assignment. If, as currently planned, this receiver operates "wideband" all the time, a more stringent assignment criterion will need to be applied and a greater rate of assignment failure will result.

- 2. Only one test environment, the Southwest U.S., was used to exercise the assignment model. It is expected that upon exercising the Northeast U.S. environment, a higher rate of assignment failure will occur. This is anticipated due to the greater numbers (4X) of preassigned ILS facilities and a greater density of enroute TACAN and VOR facilities in that area.
- 3. The channel plan used to exercise this particular trial channel assignment contains rigid frequency-pairing requirements throughout the C, L, VHF, and UHF bands. Other channelization schemes may contain selective frequency-pairing options that could results in a higher rate of assignment success.
- 4. Consistent with traditional L-band channel assignment techniques, potential ground-to-ground interactions between Y-mode DME's and X/XZ mode DME's were not considered in this trial assignment.
- 5. The protection criteria necessary for wideband PDME transponder operations have not yet been determined nor applied in this model.
- 6. Refinements in the protection criteria being established by the revised (draft) VORTAC National Standard had not been incorporated into the model at the time of its initial exercise. These refinements could result in a greater rate of assignment failure for all types of L-band equipments with the exception of TACAN-to-TACAN interactions.
- 7. The present protection of the MLS angle-guidance 3° (small community) system is considered to be conservative. The protected service volume was extended from $^{+}10^{\circ}$ to $^{+}40^{\circ}$ in azimuth to afford protection for the fly-left/fly-right pulses. Refinement of this technique may result in a greater number of successful C-band assignments.
- 8. Experimentally determined C-band and L-band protection criteria will eventually replace the analytically determined values of APPENDIX C. This may alter the assignment results.
- 9. Propagation predictions for calculating D/U values were based on smooth-earth terrain. That is, terrain shielding effects were not considered. This represents a "worst case" propagation prediction.

10. The equipment operational parameters (power levels, antenna gains) and antenna patterns listed in the MLS data base were chosen to represent a conservative but realistic working environment. The actual working environment may contain a wider range of values than was exercised in this assignment.

Appendix A

APPENDIX A

ANALYSIS APPROACH FOR DETERMINING MINIMUM D/U VALUES

The MLS intersite analysis examines the interference potential between two equipments and determines the minimum, i.e., worst-case, desired-to-undesired signal power ratio, D/U, within the service volume of either equipment. Because of the tailored service volumes and directional antennas associated with MLS and ILS equipments, a more rigorous analysis technique is required to find the minimum D/U than has been developed for circular service volumes. The approach used is to calculate the D/U at predetermined test points/locations within the service volumes, and then choose the smallest value. The accuracy of this method depends on choosing the correst test points for consideration.

The following equation was used to calculate the desired-to-undesired signal power ratio (D/U) at a victim receiver:

$$D/U = [G_{D} - VG_{D} - HG_{D} + EIRP_{D} - PL_{D}]$$

$$- [G_{U} - VG_{U} - HG_{U} + EIRP_{U} - PL_{U}]$$
(A-1)

where

D/U = desired-to-undesired power ratio, in dB

G = mainbeam antenna gain of the desired (D) or undesired (U) equipments, in dBi

VG, HG = the normalized vertical and horizontal antenna gains (desired or undesired) in the direction of the victim receiver, in dBi

EIRP = equivalent isotropically radiated power, in dBW

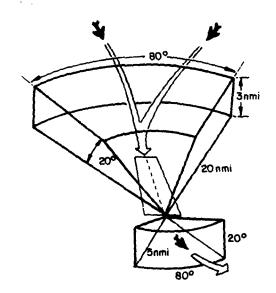
PL = propagation loss of a signal (desired or undesired) at the victim receiver, in dB.

The location of the minimum D/U value, in both azimuth and elevation, will depend upon the variation of both signals throughout the protected service volume (FIGURE A-1). From Equation A-1, it can be seen that the two main factors affecting those signal levels are propagation loss and antenna gain. Two simplifying assumptions were drawn from preliminary analysis of these variables:

1) when an undesired equipment is located outside the radius of the protected service volume, the minimum D/U location will occur at the farthest range (on the arc) of the service volume, near specific points on the arc; 2) when an undesired equipment is located within a service volume radius of the desired equipment, a conservative minimum D/U value is ensured by using the worst possible D/U value that could occur between those equipments.

The first assumption is based on the calculation of D/U values in the MLS service volume for many positions of the interfering equipments around the service volume. A subset of these D/U calculations is shown for interfering equipments positioned as in FIGURE A-2. The D/U value was calculated at eleven points on the MLS service volume. The azimuth scan beam antenna pattern of FIGURE A-3 was used for the desired signal horizontal antenna pattern, and the DPSK (Ident) pattern of FIGURE A-4 was used as the undesired signal horizontal antenna pattern. The resulting D/U values are documented in TABLE A-1. It can be seen that the minimum D/U value occurs on the service volume arc. In addition, the minimum value occurs near the corner points (1 and 9), or near the closest point to the undesired equipment, when that equipment is positioned within the angular limits of the desired service volume coverage.

To verify that these locations will yield a minimum D/U value for various equipment orientations, a second subset of calculations was performed with the same equipments oriented as shown in FIGURE A-5. The results of these calculations are shown in TABLE A-2. Again, the minimum D/U value occurs on the service volume arc, at either the corner points or the nearest point to the undesired equipment.



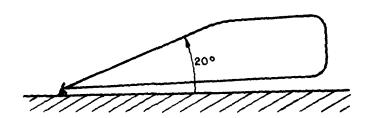


FIGURE A-1. MLS SERVICE COVERAGE.

⁶ ICAO Submission by FAA, Time Reference Scanning Beam Microwave Landing System, DOT/FAA, December 1970.

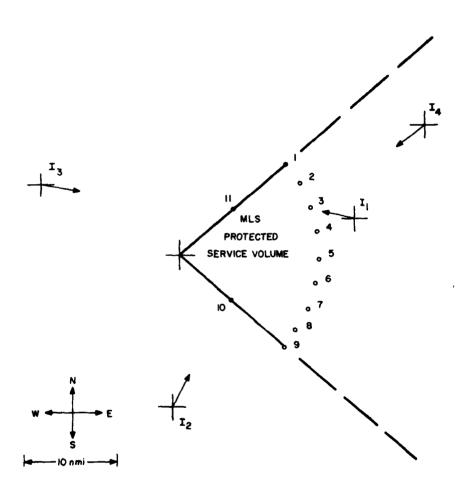


FIGURE A-2. TEST POINT LOCATIONS ON AN MLS SERVICE VOLUME.

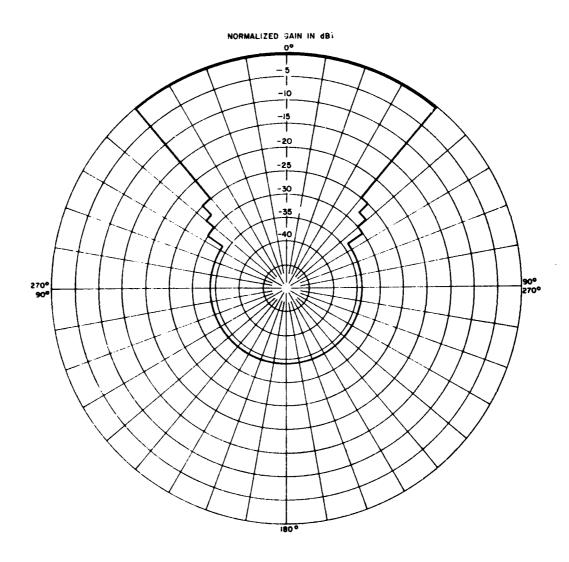


FIGURE A-3. AZIMUTH SCAN BEAM HORIZONTAL ANTENNA PATTERN.

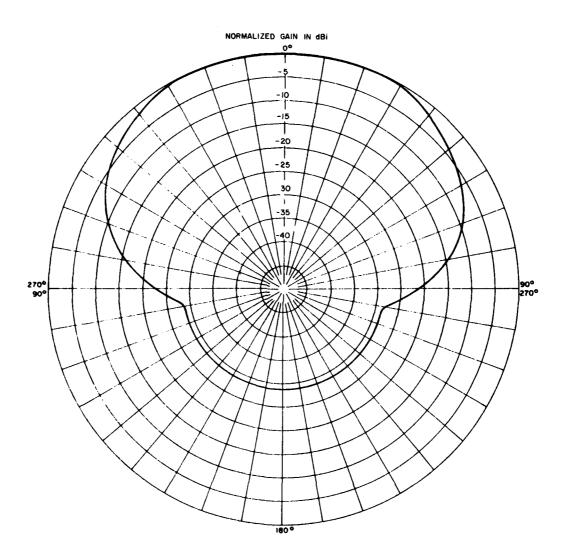


FIGURE A-4. IDENT HORIZONTAL ANTENNA PATTERN.

TABLE A-1
CALCULATED D/U VALUES

		Inter	ferer	
D/U @ (dB)	I ₁	I ₂	I ₃	I ₄
1	28.5	10.0	34.5	32.0
2	19.8	12.0	31.0	31.5
3	6.5	14.5	28.5	32.0
4	-5.8	17.0	26.0	32.0
5	~7.0	20.5	23.5	33.0
6	-4.2	24.5	20.5	33.5
7	-0.5	27.5	18.5	34.5
8	-1.5	28.5	16.5	35.0
9	-3.0	31.5	14.5	36.0
10	9.2	15.9	19.0	38.3
11	13.7	18.1	24.5	35.7

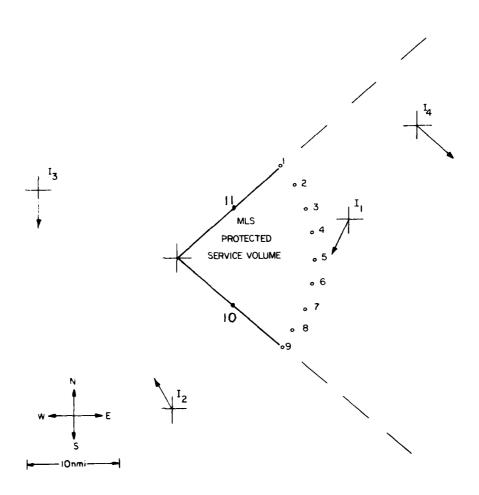


FIGURE A-5. ALTERNATE INTERFERING ORIENTATIONS.

TABLE A-2
CALCULATED D/U VALUES

		Interf	erer	
D/U (dB)	I	¹ 2	13	I ₄
1	-0.5	7.8	6.5	3.0
2	-5.2	7.8	7.0	2.5
3	-7.5	6.5	7.5	3.0
4	-8.8	6.0	8.0	3.0
5	1.0	5.5	8.5	4.0
6	7.8	5.0	8.5	4.5
7	14.5	4.5	8.5	5.5
8	16.5	3.5	8.5	6.0
9	18.0	2,0	8.5	7.0
10	13.2	7.9	12.0	13.3
11	6.9	12.1	12.5	11.7

The approach used to calculate these D/U values takes into account the vertical as well as the horizontal antenna variations and propagation loss. This is done using a propagation model developed by the Institute for Telecommunication Sciences (ITS) (Reference 4). This model calculates a D/U value versus equipment separation distance on a 95% time availability basis, based on the propagation losses and normalized vertical antenna gains of the desired and undesired signals in the direction of the victim receiver. This D/U does not account for differences in the equipment power or the normalized horizontal antenna gains. The overall D/U value is determined by correcting the ITS-calculated D/U (D/U $_{\rm ITS}$) for the differences in transmitter power and horizontal antenna gains of the desired and undesired signals. Rewriting Equation A-1 in terms of the D/U $_{\rm ITS}$:

$$D/U = (G_D - HG_D + EIRP_D) - (G_U - HG_U + EIRP_U) + D/U_{ITS}$$
(A-2)

where

D/U_{ITS} = the ratio of desired to undesired signal propagation loss and vertical antenna gains, for a fixed desired-to-undesired separation distance and victim receiver altitude, in dB.

$$D/U_{ITS} = VG_U + PL_U - VG_D - PL_D$$

It can be seen that the $\mathrm{D/U}_{\mathrm{ITS}}$ contains those variables, i.e., propagation loss and normalized vertical antenna gain, that vary with respect to the altitude of the victim receiver. To ensure that the overall $\mathrm{D/U}$ value is minimized with respect to altitude, the $\mathrm{D/U}_{\mathrm{ITS}}$ is calculated at the worst-case altitude, for each value of separation distance, and these values are stored in look-up tables for use later in calculating the overall $\mathrm{D/U}$.

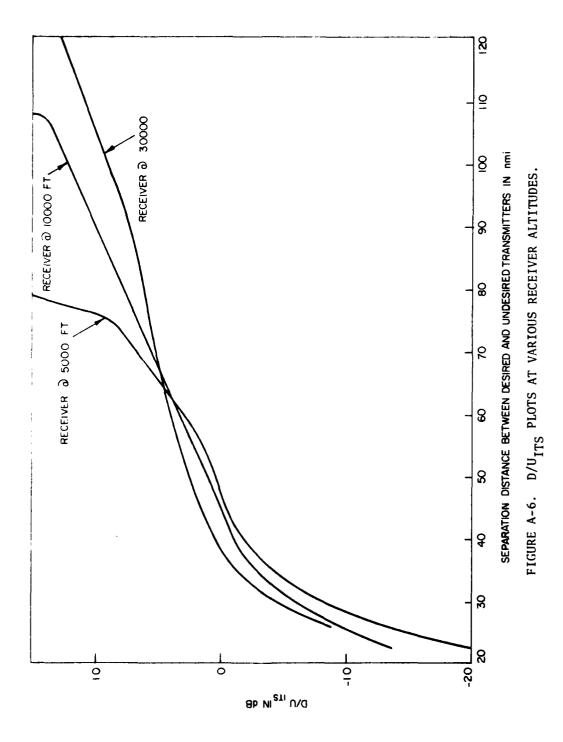
The separation distance is the ground distance from the undesired equipment to the victim receiver, plus the ground distance from the victim receiver to the desired equipment.

The process of creating these $\mathrm{D/U}_{\mathrm{ITS}}$ look-up tables is based on producing a series of $\mathrm{D/U}_{\mathrm{ITS}}$ curves for several altitudes within the limits of the victim's service volume, and combining these curves by taking the minimum value at each increment of separation distance.

FIGURE A-6 shows a series of D/U $_{\rm ITS}$ curves for a victim receiver at 20 nmi from the desired equipment and at various altitudes. It can be seen that the minimum D/U $_{\rm ITS}$ will occur at higher altitudes for increasing values of separation distance. By combining these curves, taking the minimum D/U for each value of separation distance, it is possible to produce a single curve that minimizes both the propagation loss and vertical antenna gain ratios for the desired and undesired signals (FIGURE A-7). Using this curve, in a tabulated form, the intersite model obtains a D/U $_{\rm ITS}$ value that reflects the minimized propagation losses and vertical antenna gains by calculating the separation distance through a point on the service volume arc, and obtaining the corresponding D/U $_{\rm ITS}$ value from the proper look-up table.

The second assumption is based on the premise that, by assuming that the worst-case interference will occur when an undesired equipment is located within the circle inscribed by the victim's service volume radius, a conservative minimum D/U value will be used for all those equipments. This worst-case interference is defined by the equipment protection criteria (Appendix C) as the lowest possible D/U value that can occur between interfering equipments. The considerations in determining this worst-case value are described in Reference 9 of Appendix C.

The overall intersite analysis approach developed as the complexity of the task involved. It was necessary to use an analysis that could universally handle all the service volumes and antenna patterns used in the assignment system, and be implemented in a reasonable time period. As the total assignment system is exercised, it may become apparent that the conservative approach used within the service volume radius restricts the assignment of equipments. Refinement of the intersite model to produce correct results for interfering equipments within the



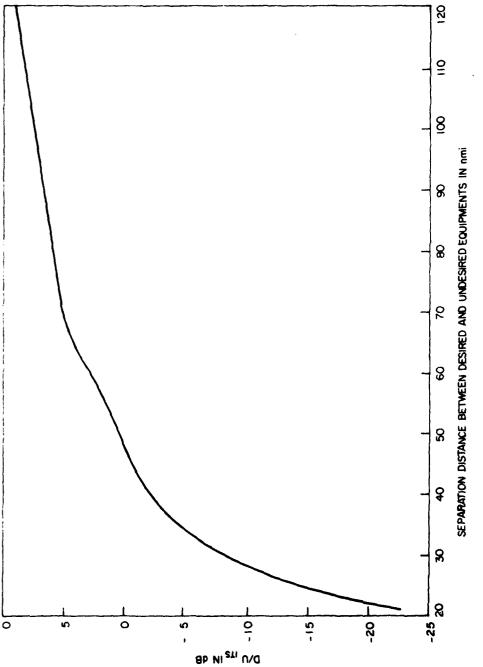


FIGURE A-7. COMPOSITE D/U $_{\mbox{\scriptsize ITS}}$ CURVE FOR 5,000, 10,000, 20,000 FEET ALTITUDES

victim service volume radius would involve calculating D/U values at a greater number of points. The scheme would be similar to that shown in FIGURE Λ -8. For the interfering equipment (I) shown, a D/U calculation would be made at several points, A-G, along the service volume radius, in addition to the points used on the arc. The number of additional calculations necessary would depend on the directionality of the horizontal antenna pattern of the interfering equipment.

In its present form, the intersite routine contains the necessary capability to accommodate a variety of refinements. As it becomes clear that additional capabilities would be beneficial, the routine can be altered.

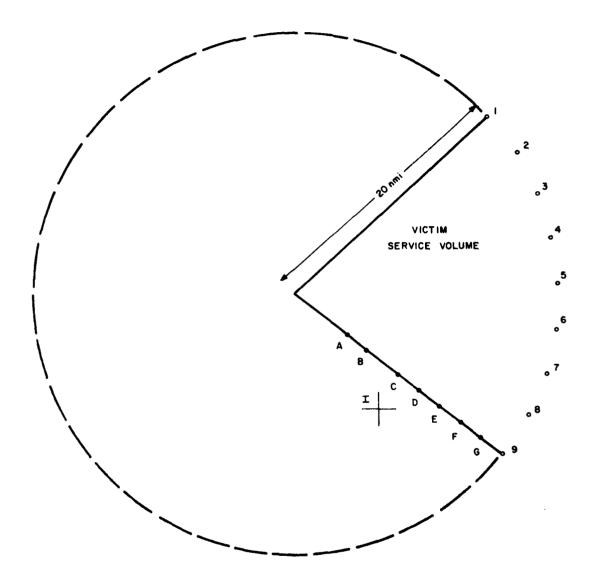


FIGURE A-8. REFINED INTERSITE ANALYSIS.

APPENDIX B

SYSTEM DESCRIPTIONS

This appendix contains a description of the Microwave Landing System (MLS) angle-guidance functions and associated Precision Distance Measuring Equipment. A section is included summarizing the functions, service options, and system parameters to be used for each equipment in the assignment model.

MLS ANGLE GUIDANCE

Angle Guidance (Reference 6)

The TRSB signal format is based on the TO-FRC scanning beam technique, in which narrow fan beams scan through the coverage volume in alternate directions. The beams are scanned at high speed and consist of a single, unmodulated, continuous radio frequency transmission. The scanning speed is uniform, starting from one extremity of the coverage sector and moving to the other and then back again to the starting point, thus producing a TO-FRO scan as shown in FIGURE B-1 for azimuth. The azimuth beam scans first counterclockwise and then clockwise, as viewed from above. The elevation beam scans first down and then up. In every scanning cycle, two pulses are received by the aircraft. The time interval between the TO and FRO pulses is proportional to the angular position of the aircraft with respect to the runway centerline. An important feature of the time reference encoded scanning beam system is the high data update rate, 13.5 Hz for azimuth and 40.5 Hz for elevation. These data rates make it possible to design simple airborne processors that can minimize multipath effects on guidance signals.

All angle and data functions are time-multiplexed on the assigned radio frequency so that a single receiver-processor channel may process all data. Since each function is an independent entity in the time-multiplexed function sequence, the receiver may decode functions in any sequence. This is accomplished by providing each function with a preamble that, upon reception, sets the receiver for the function which follows. The function identification preamble is radiated on

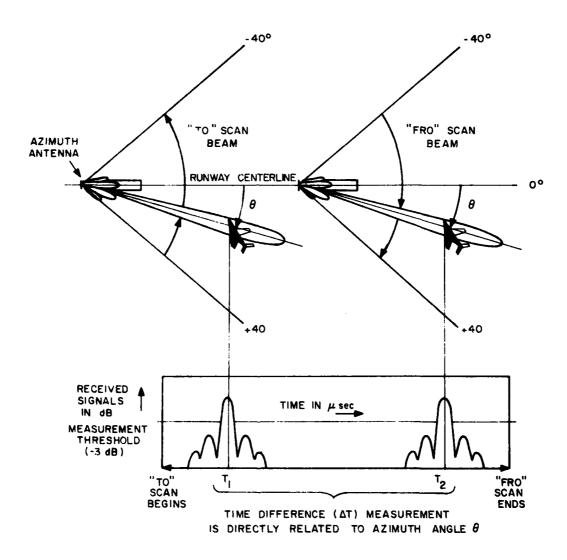
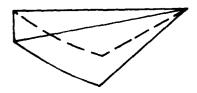


FIGURE B-1. TIME DIFFERENCE MEASUREMENT.

a sector antenna covering the function guidance volume. The scanning fan beam and the sector transmission are illustrated in FIGURE B-2.



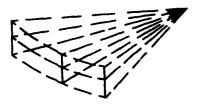


FIGURE B-2. REPRESENTATION OF THE ANGLE AND PREAMBLE RADIATION CHARACTERISTICS.

All angular information is essentially linear throughout the volume of coverage. Precision azimuth angle guidance is provided to at least ±40°, or a narrower sector if desired. For any installation, and particularly where proportional coverage is reduced for reasons of economy, left-right guidance information may be provided over a wider sector. Precision elevation angle guidance, referenced to a standard reference point, is provided from 1° to 20° in elevation, over the same sector that provides azimuth angle guidance. Precision missed-approach azimuth angle guidance, referenced to runway centerline, is provided to at least ±20°.

The proposed standard signal format contains a time slot for the addition of 360° azimuth and missed-approach elevation guidance to meet potential future requirements, and the design concept is sufficiently flexible to permit the implementation of alternate means for providing a 360° azimuth capability for particular national requirements. Such an alternative could be implemented at C-band or Ku-band with either electronic or mechanically scanned antennas and could be made compatible with standard receivers by a simple processor augmentation.

Signal Formata

The TRSB signal format defines details of the signals-in-space provided by MLS. The unique signal format concepts affecting operational and performance characteristics of TRSB are discussed below:

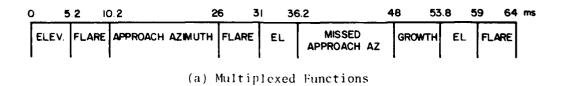
- 1. 200-independent-channel capability for angle and range.
- 2. Time Division Multiplex (TDM) operation of all TRSB functions per channel such that only one MLS transmitter is operational at any one time and only one receiver processor channel is required to decode angle guidance information.
 - 3. A large number of samples per second to permit data averaging.

By employing the TDM format with a unique identification for each function, functions can be easily added to or deleted from the signal format to accommodate specific runway requirements. In this way the format provides a high degree of flexibility and growth capability to accommodate potential future requirements for additional MLS functions or auxiliary data messages. Functions provided by the signal format are:

- 1. Function preamble including function identification.
- 2. Auxiliary data (e.g., Site Geometry, Status of Subsystems, etc.).
- 3. Approach azimuth angle guidance.
- 4. Elevation angle guidance.
- 5. Missed-approach azimuth angle guidance.
- 6. Missed-approach/departure elevation guidance.
- 7. Flare angle guidance.
- 8. 360° azimuth guidance.
- 9. left-right guidance.
- 10. Sidelobe suppression.
- 11. Ground test signal.
- 12. Independent range guidance.

 $^{^{\}mathrm{a}}_{\mathrm{pp}}$ 1-2.5 to 1-2.7 of Reference 6.

Part of a typical scan cycle is shown in FIGURE B-3. Each function is transmitted in time sequence and is differentiated from other functions by the function preamble preceding each function transmission. The preamble is radiated throughout the coverage volume on a sector antenna and contains function synchronization and identification information in the form of differentially phase-shift-keyed (DPSK) digital signals. This function preamble is followed by left-right guidance pulses, sidelobe suppression pulses, ground test pulses, and TO-FRO angle fan beams.



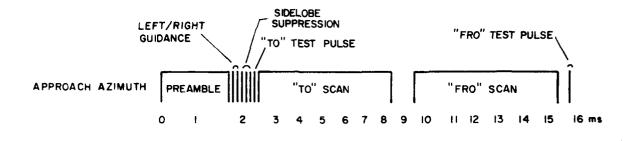


FIGURE B-3. TIME DIVISION MULTIPLEX OF FUNCTIONS

(b) Sequence for Approach Azimuth Function

Angle guidance information is derived from narrow scanning fan beams. These beams sequentially encode all angles in the coverage sector. All other functions (function preamble, auxiliary data, etc.) are broadcast on wide-coverage sector antennas.

Another key feature of the signal format is the high data rates provided to permit data averaging. This averaging reduces the effect of in-beam multipath signals which cannot be eliminated by other forms of receiver processing. High sample rates are realized with electronically scanned antennas.

The signal format is designed such that at a runway providing maximum MLS service, all angle functions are combined on a single-frequency channel, while airports with more modest service requirements use the same signal format but radiate only selected functions. This flexibility provides for complete inter-operability of all ground and airborne equipments, with the resulting service limited by the lesser capabilities of either the ground or airborne equipment.

Configurations

There are six MLS system configurations designed to provide a variety of performance levels to meet the needs of civil and military users. The three civil systems are the Small Community, the Basic and the Expanded. The remaining three systems are future military systems. At present the basic civilian system fulfills the requirements of fixed military bases. The performance capabilities of the civilian systems are shown in TABLE B-1.7

The Small Community configuration provides a minimum level of service, limited proportional or angle guidance, and less stringent accuracy requirements. The Basic configurations have several azimuth and elevation antenna beamwidth options. The wide aperture antenna configuration provides narrow beamwidths yielding higher accuracy. The narrow aperture antenna configuration provides broader beamwidths with lower accuracy. The Expanded configuration provides the complete range of angle coverage available including flare touchdown guidance, and missed approach or back azimuth.

⁷National Plan for Development of the Microwave Landing System, FAA-ED-07-2A, DOT/FAA, June 1978.

TABLE B-1

PERFORMANCE CAPABILITIES OF MLS CONFIGURATIONS (FROM REFERENCE 7)

Configuration				Basic	ر			
Function	ES	Expanded		Wide Aperture	1	Narrow Aperture	S	Small Community
	ВМа	Coverage	BW	Coverage	BW	Coverage	BW	Coverage
Azimuth	1。	+40°	1,	±40°	5.	±40°	3°	±40°
		proportional guidance		proportional guidance	_	proportional guidance		proportional guidance ±40° sector guidance
Elevation	1,	0° to 20°	10	0° to 20°	1.5°	1.5° 1° to 10°	2°	1° to 10°
		proportional guidance		proportional guidance		proportional guidance		proportional guidance
Flare	0.5	8 feet above	NA	NA	NA	NA	NA	NA
		runway to 8.5° proportional guidance						
Missed Approach Azimuth	33°	proportional guidance	KN	NA	N A	NA	NA	NA
Identification	NA	±40°	NA	±40°	NA	±40°	NA	±40°

^aAntenna - 3 dB beamwidth.

MLS PRECISION DISTANCE MEASURING EQUIPMENT

The MLS Precision Distance Measuring Equipment (PDME), operating in the 960-1215 MHz region, is an evolution of the conventional DME system. Increased accuracy is gained through pulse shape modification. As with conventional DME, the system consists of a transponder on the ground and an interrogator in the aircraft. Distance information is derived in a manner similar to that of the conventional TACAN/DME system.

The PDME is designed to be completely interoperable with conventional DME equipments and should meet the increased operational requirements that the MLS angle-guidance functions demand, which are an order of magnitude greater than those placed on the conventional DME.

To obtain the ±100 feet range accuracy necessary during Category III^a landing, modification of the signal format and design of the conventional DME equipment was necessary. The signal format was modified by sharpening the leading edge of the first pulse of each pulse-pair. The cos/cos² pulse shape chosen has a cosine shape for the leading edge of the first pulse and a cos² or gaussian shape for the trailing edge.

The conventional DME equipment concept was modified to allow for the detection of the sharper rising pulse, to more closely control the system delay time, and to improve rejection to co- and adjacent channel signals.

The PDME is a multimode system capable of operating with various pulse-pair spacings for both the ground-to-air and air-to-ground transmissions. The PDME can be multiplexed onto available DME channels in X- and Y- modes.

SYSTEM PARAMETERS

This section summarizes the important equipment functions and operational parameters necessary to exercise the channel-assignment model. The actual

and feet ceiling, 0 nmi visibility.

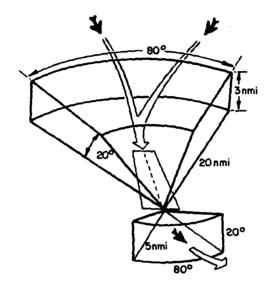
working environment may contain a much wider range of parameters than detailed here. The information in TABLE B-2 was chosen to represent a conservative but realistic working environment. The choice of functions and parameters to determine worst-case situations as well as the protection criterion is described in APPENDIX C.

TABLE B-2

EQUIPMENT PARAMETERS

Fquipment	Function	Configuration Option	Service Volume Options	Frequency	Vertical Antenna Pattern	Horizontal Antenna Pattern	ERP (dBm)
MLS Angle Guidance	Ident.	Sm. Comm. Basic	Figure 8-4	5.0-5.25 GHz	Ident. Elevation Figure B-5	ldent. Azimuth Figure 8-6	0.64.
	Azimuth Scan-Beam			S.0-5.25 GH:	Scan-Beam Elevation Figure B-5	Scan-Beam Azimuth Figure B-7	54.0
ILS	Localizer	Standard Option 1 Option 2	Figure B-8	108-112 MHz		Wilcox Figure 8-9 or 8-Loop	62.0 or 54.0
	Glideslope			331-534 MHz	9 TSO	Figure B-10 Null Figure B-11	12.3
VOR	_{NA} a			108-112 MHz			16.0 or 34.0
TACAN	NA	High Low Terminal	Figure B-12		RTA-2 Figure B-13	Omni- direction	73.0
DME	VOR/DME			960-1215 MHz	CHU Eigure B.14		13.4
	ILS/DME	Approach And Landing	Figure B-8		77 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	,	31.4
PDME	MLS/DME	Approach And Landing	Figure B-15		PDME Figure B-16	Omni/Sector	55.5

^aNA - not applicable.



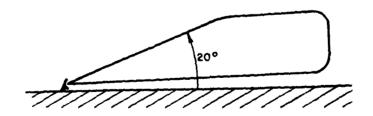
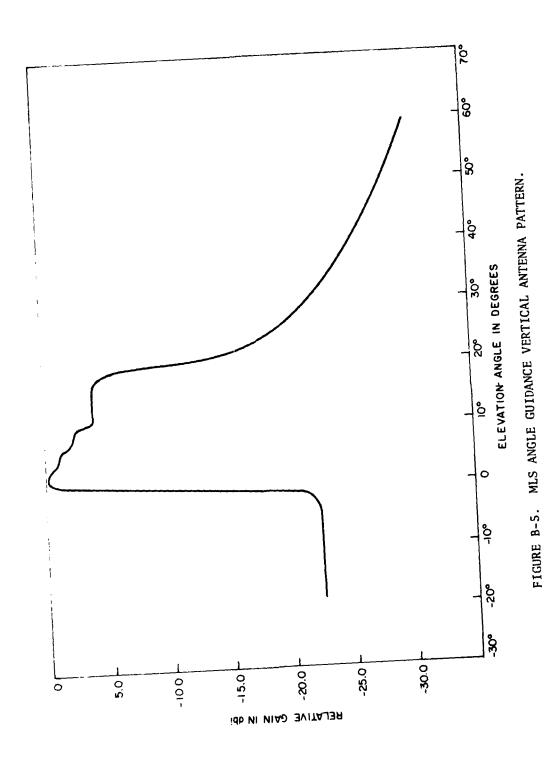


FIGURE B-4. MLS SERVICE VOLUME CONFIGURATIONS.



B-12

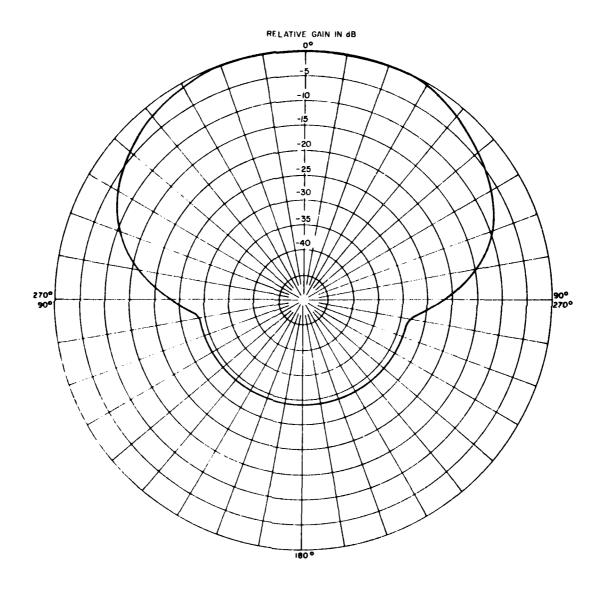


FIGURE B-6. IDENT HORIZONTAL ANTENNA PATTERN.

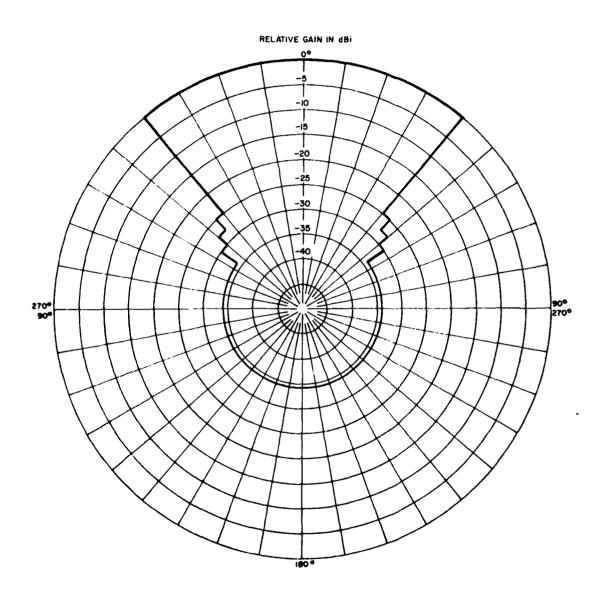
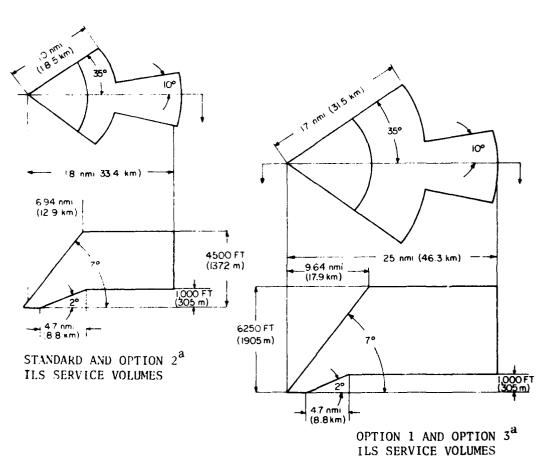


FIGURE B-7. AZIMUTH SCAN-BEAM HORIZONTAL ANTENNA PATTERN.



OPTION 2 PROVIDES THE FULL FRONT AND BACK COVERAGE SHOWN

FIGURE B-8. ILS SERVICE VOLUME OPTIONS.

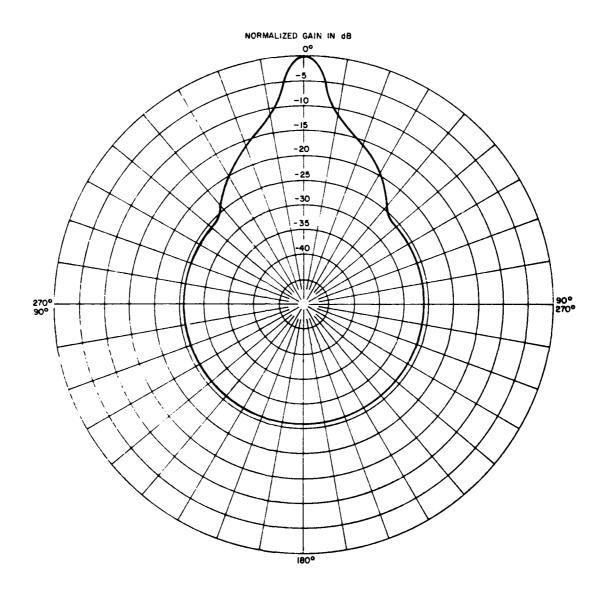


FIGURE B-9. ILS (WILCOX) HORIZONTAL ANTENNA PATTERN.

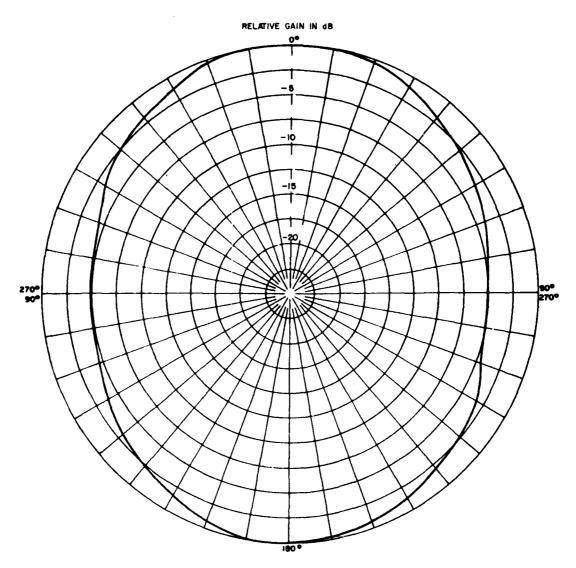


FIGURE B-10. ILS (8-LOOP) HORIZONTAL ANTENNA PATTERN.

FAA-RD-80-91 Appendix B

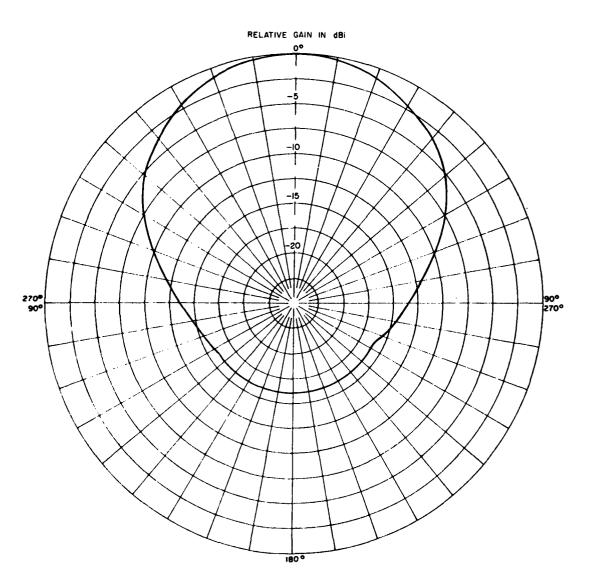


FIGURE 11. ILS GLIDESLOPE ANTENNA PATTERN.

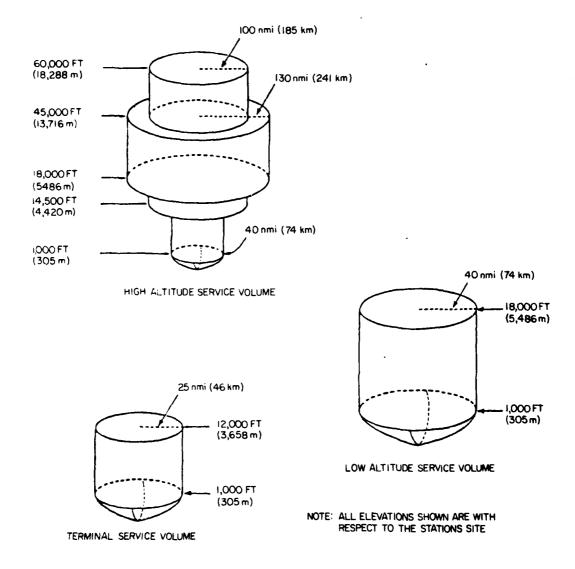
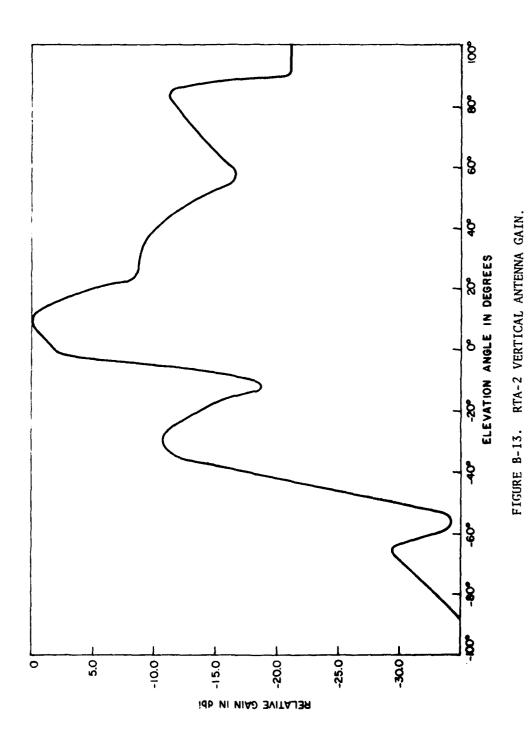


FIGURE B-12. L-BAND SERVICE VOLUME OPTIONS.



B-20

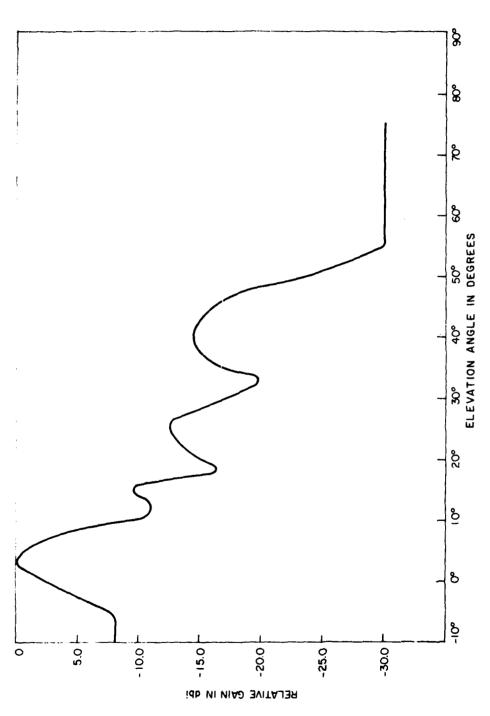


FIGURE B-14. CHU VERTICAL ANTENNA PATTERN.

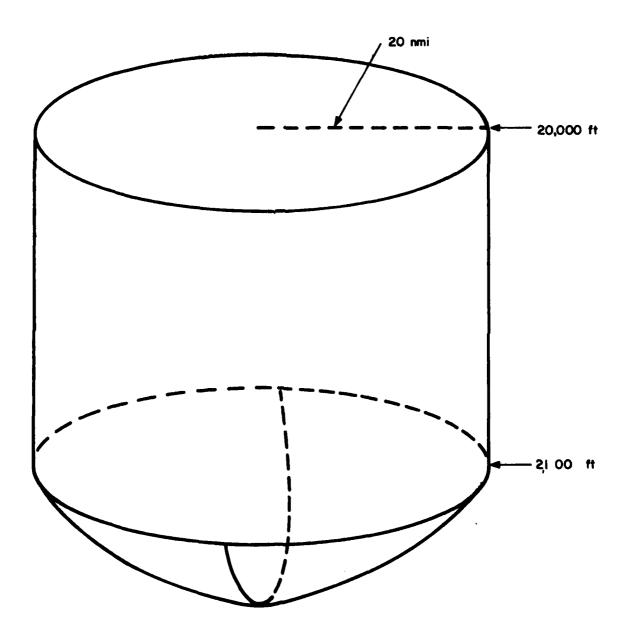


FIGURE B-15. PDME SERVICE COVERAGE.

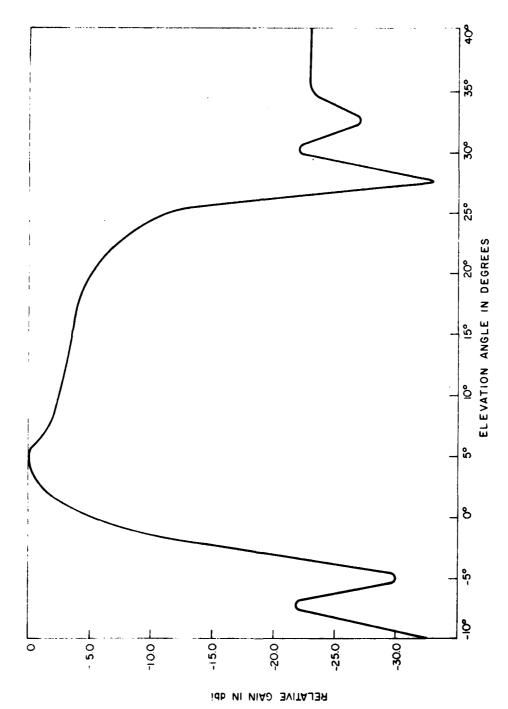


FIGURE B-16. PDME VERTICAL ANTENNA PATTERN.

APPENDIX C

EQUIPMENT PROTECTION CRITERIA

The MLS frequency-assignment model calculates the worst-case desired-to-undesired signal power ratio within the service volumes of each pair of equipments operating in the same band. It then determines the channel separation required for safe operation of each equipment pair based on the protection criteria input by the user. A different protection criterion is specified for each of the four bands to be assigned (C-band, L-band, VHF band and UHF band). In each case the criterion establishes the minimum D/U level allowed for the cochannel and adjacent-channel operation of equipments in these bands.

L-band contains three interacting types of equipments (DME, PDME, and TACAN). The operation of these equipments is such that D/U enhancement can be obtained by varying pulse-pair spacing, as well as by off-tuning. The L-band protection criteria reflects this added interference rejection by specifying D/U threshold levels for out-of-aperture (different pulse-pair spacing) interference as well as coaperture (like pulse-pair spacing) interference.

In C-band, MLS angle guidance is composed of many separate functions (elevation, azimuth, preamble, etc.) multiplexed onto a single frequency. In establishing a C-band protection criteria, it was necessary to determine which interaction of functions would cause the worst D/U degradation. It was found that for cochannel operation, the worst degradation was for a 3° azimuth scanning beam interfering with a 3° azimuth scanning beam. For adjacent-channel interactions, the worst degradation was for a preamble function interfering with a 3° azimuth scanning beam. This type of criterion requires that two worst-case D/U values be considered in the intersite analysis, scan beam-to-scan-beam for cochannel comparison and preamble-to-scan-beam for adjacent-channel comparison.

TABLES C-1 through C-4 list the protection criteria used in this particular trial assignment.

TABLE C-1

L-BAND PROTECTION CRITERIA

Frequency and Pulse-Spacing Interaction	D/U Threshold (dB)
Cofrequency Coaperture	+ 8
Cofrequency Out-of-Aperture	+ 3
lst Adjacent Frequency Coaperture	-25
lst Adjacent Frequency Out-of-Aperture	-34
2nd Adjacent Frequency Coaperture	-34
2nd Adjacent Frequency Out-of-Aperture	-34

Nanda, V. P., Analystic Determination of Interference Thresholds for Nicrowave Landing System Equipment and TACAN/DME Equipment, ECAC-PR-80-008, Annapolis, MD., to be published.

TABLE C-2

C-BAND PROTECTION CRITERIA9

	D/U Threshold
Cochannel	23.5 dB ^a
lst Adjacent Channel (±300 kHz)	-19.4 dB
2nd Adjacent Channel	-26.0 dB

^aRecent tests at NAFFC have indicated that cochannel protection requires an absolute limit on the undesired signal of \approx -103 dBm. The CAM will be revised to include this new type of protection criteria.

TABLE C-3

VHF BAND PROTECTION CRITERIA¹⁰

	D/U Threshold
Cochannel	20 dB
1st Adjacent Channel (±50 kHz)	~ 7 dB
2nd Adjacent Channel (±100 kHz)	-46 dB
3rd Adjacent Channel (±150 kHz)	-50 dB

TABLE C-4

UHF BAND PROTECTION CRITERIA¹⁰

	D/U Threshold
Cochannel	20 dB
lst Adjacent Channel (±150 kHz)	0 dB
2nd Adjacent Channel (±300 kHz)	-20 dB
3rd Adjacent Channel (±450 kHz)	~40 dB
4th Adjacent Channel (±600 kHz)	-40 dB

⁹Nanda, V. P., Analytic Determination of Interference Thresholds for Microwave Landing System Equipment and TACAN/DME Equipment, ECAC-PR-80-008, Annapolis, MD., to be published.

¹⁰Order 9840, Selection Order: U.S. National Aviation Standard for the VOR/DME/ TACAN System, U.S. DOT/FAA undated.

APPENDIX D

TRIAL ENVIRONMENT

This appendix contains a listing of the airport and enroute environments used in the trial assignment. Listed along with each system is its present operating channel (if it is preassigned), and the channel assigned to it by the assignment model.

TABLE D-1 summarizes the number of individual equipments of each type included in the environments listed in TABLES D-2 and D-3.

TABLE D-1
TEST ENVIRONMENT SUMMARY

Facility	Existing Requirements	New Requirements ^a	Total
TACAN	118	0	118
DME	137	28	165
V OR	169	0	169
ILS	86	0	86
MLS Expanded	o	5	5
MLS Basic	0	136	136
MLS S. Com.	0	214	214
MLS PDME	0	66	66

Note that frequency-pairing requirements within a particular channel plan may necessitate the protection of new "dummy" DME. VOR and ILS equipments whenever MLS equipments are assigned which do not require the physical installation of associated equipments. These dummy equipments are not included in the tables.

TABLE D-2

AIRPORT ENVIRONMENT (Page 1 of 8)

SYSTEM IDA	LOCATION CITY/STATE	æ ∺ E	FAC	AIRPORT TYPE	FAC LATITUDE		FAC ONGITUDE	S A N	EXIST	MLS Service	1 C E	OME EQUIPMENT	× 120	Faurp &	L INK NU"	CHANNEL OLD/NE	E C
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۰ ۱		VCA			*	~	7 55 00	1,4			COMNIY	MARKER BECN				`	
n •		V (;	٠,	4	z	7 55 03	54			COMNIT	MARKER BECA				`	95 Y
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œ		/C.A	> > ∀	AILCBR	S.	مر ا	4 06 33	; ~	, ,	SMALL	COPNIY	ILS ONE		٠ ١		1407	× × × ×
	AUBURN MUN/CA	/ C A	A O &	9	57	~	1 34 51	1	S	SHALL	COMNIY	ILS DME				. `	184
	AVALON	/CA	AVX	S	*	~	8 24 53	22	s		COMNIY	80				`	23 V
	AVALOR	V (X A X	· •	5	-	6 24 53	£ 7			COMNIY	œ				`	28 Y
	CALALINA		·	VSTOL	د. ا در ا	_ :	00 yl n	27		SMALL	CONVIX	~				`	52¥
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	BISHOP	/C A	_	GENERAL	22		8 21 54	3.0	2 10	SMALL	COMNIY	MARKER BECK	c	1	-	\ \ \ \ \ \ \ \ \ \ \ \ \ \ \ \ \ \ \	28.4
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	# : K : C			GENERAL	25	~ ·	2 59 7	13			COMNIT	MARKER BECK				7	111
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	COLUSA LUI		. A.O.		7	- · - ·		2.5	Y E		COMPT	MARKER BECK				`	78Y
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(Page 2 of 8)

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23	÷	FCH		36 43 57	H 10 66 011 4	21	SMALL COM	MARKER	BECN			`	20Y
25	FULLERIN ACA	<u>.</u>		13 52 19	3 44 85 41 N	9 ;	BAS WICE	BAZ P DME				•	232
n de	-	100	TAN GENERAL	20 25 19	3 44 80 71 T	* *	YES BAS MIDE BAZ	MAD ONE	10			•	766
55	SRASS VLL /CA	617			N 121 00 15 W	. ~		ILS DME				`	384
9.	SRASS VLL /CA	017	ی	39 13 25 1	W 121 00 151 W	1.5	SHALL	_	EC.			`	RIY
25	HALF MOONS Y/CA	nAF	19	37 30 50	v 122 30 23 W	30	SMALL	_	100			`	2.8 Y
æ (HALFMOOREY/CA	HAF	ENS GENERAL	,	W 122 30 00 W	9	SWALL	_	NO 30			`	¥04
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6.3	HAY WARD ATTCA	3		37 30 34 1	N 122 67 19 19	101		3#13				. `	392
•	HAYBARD AT/CA	Ç,	Ç	37 39 34 1	W 122 07 18 W	286	BASIC	POPE		QAH S		52X/	\$2x
65	HENET RYAN/CA	HAT		33 44 06		23	SMALL	IY MARKER	PECK			`	496
99	HOLLIST MU/CA	307	ی	36 53 25	N 121 24 39 W	12	SMALL	MARKER	BECN			`	54.7
67	HUNEROTOR /CA	11.	EXS SEVERAL	33 43 68 3	3 2 2 2 3 1 3 A	- ;		FARKER	SECN			`	:
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TABLE D-2

(Page 3 of 8)

SYSTEM ID®	LOCATION CITY/STATE	_ <u>w</u>	FAC	AIRPORT TYPE	*3	FAC LATITUDE		FAC LONGITUDE	#61T	JOE	EAN	RNET		MLS Service	_	DAE Equipaent		11.5 g	FOUIP	LINK CHANNEL NUM OLD/NEW	CHANNEL OLD/NEV	EL
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201	MANNOTH INCO	55	1	NES GENERAL	50	2	2 Z	-	4 4	37	52	2 2	SMALL	COMMIT		KARKER	BECK				` `	25Y
12	MERCED MUN/CA		HC F		'n	; ;	9	2.5	90	3 %	P 69	YES			_		שני ב היות היות		40	7	, XU X	1 7 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1
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112	WC1TEBELLO/CA	40			4	C	2 00	1 18	36	30	00	N.				MARKEP BECK	SECA				`	297
113	MONTE BELLOZCA	4			40	33	200	3 I	9.	33	21	O.¥		COMMIT	>-	WARKER EECN	EECN				`	26Y
ø ,	WOLFRENCE POLICE	4	۲ ۲		<u>.</u>	#)	7	121	-	23	61	YES		3014 3		DINE O			404		38X/	38X
(D)(VO/A ABAGINOM	5	> ~ 3.		36	W: 1	z :	121		MO A	9 ;	YES		101		P CPE					`	252
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TABLE D-2 (Page 4 of 8)

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MLS SERVICE	5	105	֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓			0				VIDE		ទី	1010 V 1	3017	10.	100	2 5	3 6	2 5	1 2	2 5		2 6	1 6	2 6	IDE	105	101	10.	105	301	1 5	100	10E	105	301	1 5	1 1 2	101	101	IDE	106	W10E	2 6	102
MLS SER	A L	2 z	CHALL	SMALL	SMALL	SMALL	BASIC	SHALL	SMALL	BASIC	BASIC	SMALL	س	BAS					040																										
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AIRPORT TYPE	39	7 7		9	GE.	GE		9	¥	AIR	4					į				=			3	Ē	ī	*	ī	Ë	==	# :			Ī	Ĭ	=				=	ij	Ξ	=		=	Ī
¥ F	Ex3	SXS	X X	Exs	EXS	2 × 3	3	SX3	EXS	Exs	Exs	27 C	2	2 2	2 2	Z Z	2 2	2 2	2 2	2 2	2	22	2 2	, X	EXS	EXS	Exs	Exs	Exs	EXS	EXS	N X X	Exs	EXS	EXS	XX		, v	EXS	EXS	CX2	ExS	SXX	2 2	S
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¥ #	ALE/AZ	142	7	142	?	142	747	112	142	7	7	?;	3	CASILE AFBICA		TRAVIS AFBICA	TO COMPANY OF THE PARTY OF THE	5 5	5 5	5		WATHER AFRACA	5	2	2	70/	DAVIS MONT/AZ	1 4 2	Z.	٠	5 ;	֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓	INPERIAL B/CA	GEORGE AFE/CA	LEMOORE /CA	LIBST AAF /AZ	MOSTN 152 M/CA	1	SAK CLEMEN/CA	SAN NICOLS/CA	Ş	182	??	3	AF B / NV
LOCATION CITY/STATE	_							_	-							4		TABLE AFAC	CA GRANTER	•		45	*	4	z	_	FCN1	ş	80	٤.	CKOMSCARO THE COMPANDA	41 TZSCHF	_ =	AF.		4	ž	J/ ngns Ld	1	20.5	4 %	.	\$	AF	¥
114,	SCOTTSD	200	SON	SON	SOM	SON	SON	20	Sro	۷	4	٠.		֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓		7 5	2		1			, e	. A	NO	HAVILTON	TOR	15	Ξ	4	٠ ج	CKOMSCARO F: CSTATES	725	ER 1	30	0 2	94	. z	976	2	Ξ	<u>-</u>	Z :	ALLON	FLLIS	IELL IS
U	SCO	TUCSON	Į,	TUCSON	35	ž	ž	PILLCOX	2	Y ON Y	<u>-</u>	֓֞֞֝֓֞֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓	2 .		,	X 4			1	. I			4	9	1	EL TORO	DAV	=	FILL AFB	3	֓֞֞֞֜֞֓֓֓֓֓֓֓֓֓֓֓֓֓֓֟֓֓֓֓֓֓֓֓֓֓֡֓֓֓֓֓֓֡֓֡֓֡֓֡	3 6	À	6 E0		֓֞֞֜֝֟֓֓֓֟֝֟֓֓֓֟֟֓֓֓֟֟֓֓֓֟֟	200	1	SAR	SAR	SAR	LUKE AFB	51		E
1 E H	10	302														_ 0	9 0									88			331		2 =	5	36	37	æ e	6	: =	2	343	;			348	2	2
SYSTEM IDS	ñ	n n	้	ñ	ñ	ñ	ń	m)		(7)	ro i	m i	, ,	'n	, ;	o =	, ,	, 2	, j.	i iri	, i	'n	'n	'n	'n	'n	'n	'n	m	,	ń		m	m		٠, ١	, m	ň	ň	ň	ň	ñ,	'n	ň	n

TABLE D-2 (Page 8 of 8)

	22222
CHANNEL OLD/NEV	28x/28x 28x/28x /212 /252 /352
LINK	
ILS EQUIP LINK OPT CALL NUM	2 P40
DME	
MLS Service	BAS WIDE BAZ 360 EXPN BAZ BAS WIDE BAZ BAS WIDE BAZ BASIC WIDE
EXIST	Y Y ES
EAY	22 72
FAC LONGITUDE	112 56 00 E 118 05 01 U 118 05 01 K 118 05 01 K
FAC LATITUDE	30 12 00 X 34 53 46 X 34 33 46 X 34 33 46 X
AIRPORT TYPE	EXS MILTANY EXS MIR CANR EXS MIR CARR EXS MIR CARR EXS MIR CARR
FAC	
ON	55555
LOCATION CITY/STAT	DUSWAY PALMDALE PALMDALE PALMDALE
SYSTEM 104	20 20 20 20 20 20 20 20 20 20 20 20 20 2

TABLE D-3
ENROUTE ENVIRONMENT
(Page 1 of 4)

SYSTEM	LOCATION CITY STATE		EQUIP LATITUDE	# <u>5</u>	<u>u</u>	ند	EQUIP Longitude	73		w	EQUIPMENT TYPE	SERVICE VOLUME	CALL	CHANNEL	LINK
10008	GEORGEAB	7	*		7	2	11.7	23	2.1	3	TACAN	, C J	^ C ^	23X/ 23X	
80005	BEALE	5	39	9	96	z	121	56	~	3	TACAN	LOW LOW	848	23X/ 23X	
80003	INP BCH	5	35	"	3	2	117	96	32	3	TACAN	1.34	NRS		
		5 0	,	2	18	z :			- :	> :	TACAN		X Y	33X/ 33X	
90008	CRES LND		, P.	~	٠.	2	121		•		ACAL	101	7 X X	39X 39X	
8 2007	SNNICLIS	3	33		õ	*	-			3	TACAN	78C -1	NSI		
90006	PT #UGU	5	ň	0	2	×	119	0	-	3	TACAN	101	OTA		
6000		5	7	0	-	z	111		•	_	TACAN	LOW	41H	X64 /X64	
0010	SEAL SCH	<u>ځ</u>	7	•	S	2	118		-	_	TACAN	TERMINAL.		/×6*	
40011	CRUSLADG	5 6	~ U	* :	2:	z	121	9 :	10 H	> :	TACAN	3 : 3 : :			
31000		5 6	ה ה			.	1		٧ ٠		- A C A C A C A C A C A C A C A C A C A		012	35X 55X	
91906		5 5	2 4				٠,				7 4 7 4 7	JANIES.	202		
80015	SKILERNI	55	, 10	- 0	, 10	? Z	118	2 10	7	, >	TACAN	707	002		
80016	HAMILTON	4	38		180 180 180	z	122		-	3	TACAN	107	SRF		
80017	LUKE	4 2	33		41	2	112	22	52	3	TACAN	107	LUF		
81018	MARCHAFB	Š	۳,	R)		2	117		ľ	_	TACAN	TC7	۶ ۱ د		
00	ALAMEDA	Š	-1	•		2	122		4	'4	TACAY	1,0%	N 5 2		
90050	MATHERAB	٥ م	æ.	•		2	121		\$		TACAN	F07	ď T R	81X/ 81X	
0021	FALLON	بر	6 , 1	N.		z	118		~	-	TACAN	H16H	NFL		
0052	¥04V	4 2	32	•		2	114		•	3	TACAN	F0-	NYL	84×/ 84×	
80023	NHINHSAG	~	32	۰.		z	116				TACAN	101	OMA	111x/111x	
42000	TAN VIOLE	5	÷ :		•	2	121				PACAL	AC .	nns	113x/113x	
C 20 C C	NIN SEC	5 :	25		n i	2 . n i	11		Э,	> :	TACAN	30 . C	AZN.	117×/117×	
9000		3 6	2 5	2 6	o n	2 2	133	7 6	a (•	2404-		200	125X/125X	
200	VERNAL	3 =	9	4 0	9	2	109			. >	4 P C A	# a	9 -	1234/1234	
9001	LGSTAFF	7 Y	8	m		Z	111				VOP 1-4	101	ی ا		
90015	NOGALES	2 Y	31	~		2	110			38	VOR 1-A	TERMINAL	or s		
93016	VERTURA	7	ø	0		×	119		ı,	78	_	L-014	VIU		
90017	LAK HUGE	ا به در	4	4		2	118	₩)	H)	>	-	36.7	SHI	21X/ 21X	
9000	202	5 5		7 6	י ה	,	111	* *	-	3	٠,	JANIERA	000		
		3 5	7 4	V F	2 +	* 3	1 2 2	2 5	'n	• =	4 · · · · · · · · · · · · · · · · · · ·			21X/ 21X	
0021	CTOR MUN	5 5	11	, 4	•	2	113	10	9 6		-	101	200		
0022	SANT AN	4	#3 (4)	4		>	117			7	-	TERRINAL	N N		
90023	KINGHAN	4 Z	an Ma	15	3.8	z	113			3	VOR 1-4	L02	I G#	25 x / 25 x	
90024	DOUGLAS	74	3.	N		z	104			>		707	900		
0025	PRICE	5	6	m 1	Ö	z :	110		S.			TERMINAL	DO:	27x / 27x	
90050	### - P#0	3	•	2	6 !	2 2	120	γ.	٠,	3 :	٠,	TCR TINAL	X (
2000	CRESCENT		7 :	•	•		77		٠.		٠.	A.C.J.	י ני ני		
8200	1 A 1 K 2 K	5		n e	•	* :	611		٠,		-	100	A .		
90030	SHT CALA	50	0 M	, v	5 M	2 Z	113	2 6	200	3 3	VOR 1-A	LERRINAL	7 I X	31X/ 51X	
90031	S. RT ROS	3	*	1	1	2	122			2	-	200	212	311/ 311	
0032	BISHOP	3	37		n	2	118		ŝ	3	-	707	#16		
0033	FT JONES	5	7		ě	2	122	•	-	3	-	LO#	FJS		
4006	LOGAN	5	7	50	m.	2	111	2	5	>	VOR 1-A	TERMINAL	16 0	35X/ 35X	
90033	MOA8	5	60 F;	4	Ñ	2	104	÷	5	3	VOR 1-A	TERMINAL	OAB		

IIT RESEARCH INST ANNAPOLIS MD MLS CHANNEL ASSIGNMENT MODEL.(U) AUG 80 T HENSLER, A KOSHAR AD-A093 449 F/6 17/7 F19628-78-C-0006 NL ECAC-PR-80-012 UNCLASSIFIED 2..2 A) A) =4.545 END PATE FILMED 2 81

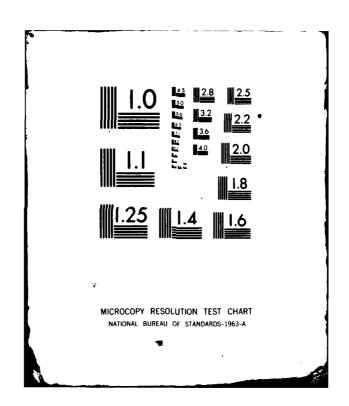


TABLE D-3 (Page 2 of 4)

SYSTEM	LOCATION		EGUIP	4			EQUIP	۵		EGUIPMENT	344	H	SERVICE	CALL	CHANNEL	E L	LIRK
å	CITY STA		A 7 1	5		2	LONGITUDE	3		_	TYPE		AOT OME	LETTERS	010	NE N	5
90836	SNT GEOG	5	1.	0.5	11	z	113	35	30	2	¥.	7	TERMINAL	02 N	35x/		
	CHCO RUN	5	5	-	ž	z	121	50.4	9	ž	~	4	TERMINAL	CIC	351/	200	
	PAXBELL	4 U	ŝ	13	5	z	122	13	2	<u>=</u>	~ ~	7	F07	2 1 2	37x/		
6000	PRIEST	5	36	8	58	z	120	39	5	<u> </u>	VOR 1	4-	L04	£0.	37X/		
9+00+	ARCATA	3	•	5	Š	2	124	. 96	# 9i	<u>=</u>	VOR 1	7	F.04	ACV	39x/	39×	
14006	BUCKEYE	5	2	2	2	z	112	. 64	2	≤	<u>ج</u>	4	 	BXX BXX	43X/	•	
	נרא	>	33	17	ě	z	114	20	2.	<u>~</u>	<u>"</u>	4	F0.7	ELY	43X/	# 2 W	
2000	SAT MONC	4 U	S	_	2	z	118	27 2	3	₹	ĭ	7	LON	SMO	45x/		
	MARYSVIL	5	5	Ę	9	z	121	3.	2	<u>×</u>	۳ ۳	7	TERMINAL	N V	45X/	¥S*	
90045	FOYTAGUE	5	7	-	2	z	122	27	20	≶	VOR 1	7	TERMINAL	λIS	45K/	45X	
\$ + 00 f.	SAT MONC	5	ŕ	Ę	37	z	118	27.	-	≆ -	۳ چ	7	30,	SMO	45X/		
90047	DISPENIE	Š	M,	5.7	0	æ	117	26.	3	¥	-	7	707	RAL	51X/		
8 4 0 0 6	POMONA	5	ø,	3	Ÿ	z	117	17	2	<u> </u>	_	4	F.0.P	#04	41X/		
64000	FORT HUA	A 2	31	e)	35	z	110	202	25	š	-	*	TERMINAL	FRU	53X/	53X	
9 2 2 2 0	VANDENBE	2	ň	4	t, G	Z	120	33	2	=	۳ ۳	۳,	F.0.	VBG	55X/	A CO	
15000	PEACH SP	77	33	3.4	53	¥	1.3	32	22	≆	~ K	4	#101#	59 6	57X/	578	
90055	FILFORD	-	8 ;	21	7	¥	113	8	3. 2.	ž	VOR 1	7	#16H	F.	58X/	58X	
90053	MAPA CC	3	₩,	2	4	ē?	122	22	0	Š	۳ ۳	7	TO.	APC	58X/	58X	
90024	ONTARIO	5	ic.	'n	69	z	117	31.4	•	ž	۳.	ą:	HIGH	0N1	29x/	59x	
0.0035	SAT MOUN	>	*	34	ď.	2	316	53	2	<u>~</u>	50	4	13 E1	B.A.M	59x/	5.9X	
	BONNEVIL	5	4	4	*	2	113	ů.	≯	-	š	7	4I6H	BVL	70X	70X	
	ST JOHNS	A 2	œ,	25	5 6	z	109	80	3	<u>=</u>	V08 1	9	#16H	SUS	7 UX/	70X	
	UKIAH FU	2	0	5	72	£2	123	. 91	2	>	£	7	416H	UKI	70X/	70X	
	SAN LUIS	2	3	u)	S	z	120	Ĉ.	= =	<u>></u>	5	7	101	SBP	71X/	71X	
	FILLMORE	3	4	51	2	z -		52	<u>→</u>	ž	~	7	70.T	* 1 4	72X/	12x	
1900	AIVSLOW	A 2	(A)	č	÷	×	113	4	2	<u>=</u>	3	7	н16н	32 11	73X/	7.5X	
	LOS BANO	٥,	(B)	4	9	2		9	3 2	<u> </u>	× ×	Ţ	70.7 CO#	₽X¥	73X/	73X	
	FFC TOW	3	.	-	4	_	116	27	2	-	٠ ج	7	₩	HEC	/**/	7 * X	
900	BRYCE CY		37	7	5		112	16	=	ž	~	4	1011	BCE	75X/	15x	
2962	LUNGIN	4		5	15	_	119	 80	>	ž	Œ,	4	H16H	FAT	76X/	76X	
20066	さんし こんか	7 V	10	, S	37	_	112	80	24 12:1	ž	e.	4	#0.1	2 09	78X/	78X	
19006	AN WAY	5		~ (* !	Z' :	118	50	7 ·	>	40%	m.	F.O.	\ N \	78X/	78X	
2000	DA66277		•	2	•	æ .			38 :	≨ ∶	~ ~	7	1517	DAG	79×	× 6×	
69806	LAK TAHO	٠	6	-	3	2		9	-	≤	۳ ۳	7	L0 1	L1	79X/	7.9×	
91036	CHAMBLER Mingin of	7		2	Ξ;	2 ;	11	56	20 :	<u>~</u> :	YOR	4	LON	Q.	80×	×oa	
		;	., :		;	.	11:	3:	- 9	- :	# :	Ţ.	TERRIBAL	A I A	81X/		
	1134 511	7 4	9 :	5	÷ :	2 :	111	•		> :	~	7	H	38.	821/	82X	
7 6 6 6		3	3 :	٠,			2	C:	2 :	> 3	1 0 A	7	1917	LAX.	837/	838	
	FULIS 01 BOKE	5 3	-	7 2		. .			2 5	> :	# 0 2 0 2 0 2 0 3 0	7 .	E .		83X	# C C	
	2000410F	5 5	2 2	2 6		2 4	122	7 7	9 9	S 3	* •	n e	. C	P76	/X+0	X .	
7000	100 7 100	; ;	, ,	3 5	3 %		777			• •	, .	r		182	100		
	at's sur	5	, ,	9 9		. 2	121	3 5	9 6	- 5	* e		* 2	1 00	7 7 0	2 4	
90874	FORTURE	3	4	9	: -		121		9 6			•					
00006	PSC07 NU	Ą			6	: 2	112	28		. 5	200		10.1		***	× ×	
90001	HAZEN	*	e,	30	ŝ		118	5		· 5	· ~	. 7	70	172	88 X /	, ×	
90002	Sh JOS H	5	37	53	S	=	121	35	2	ž _	2	7	701	200	88×/	X 60 60	
2000	TWIN PLA	3	ž	*	\$	*	115	9	200	<u>=</u>	۳ ۳	7	10	TRP	89X/	89X	
1000	BELLS	2	:	9 :	2	æ	=	80	9 !	ž	YOR 1	4	707	ראר	1468	89x	
98889	MERCED	5	31	2	2	2	128	23	3.4	ž -		<u>-</u>	#6J	MCE	89X/	89x	

TABLE D-3 (Page 3 of 4)

SYSTEM	LOCATION CITY STATE		FOUTP	25		3	EQUIP LONGITUCE	P UCE		ä	EQUIPMENT TYPE	ENT	SERVICE VOLUME	CALL	CHANNEL	LINA
90006	SUOH COS	ج	7	*	3	2	1	5	9	3	YOR	1-4	707	spo		
40087	SE SECO	ź	ž	9		2	114	16	¥,	>	V CR	1-A	#C1	ı		
90006	PASO 28	3	47 I	•	7.		150	٢,	e,			1-1	10N	8		
			ć. (5	9	25	•		1	C.	GF S		
	PALMOALF	5 5	7 4			, 2	77.	5 7		.	2 6	11	1017	4 L	715 /X16	
2600	NOW ONLY	2	, E	. "			. J.) (r			200		200	3 6		
	#0.1-C-C	Q.	-		Ē,	٠.	120	15	4	3	V CR	1 - 1	15.1	00		
	BEATTY	2	9,	4	2	~	116			>	VOR	3 - T	H16H	PTY		
0095	CAS GRIND	A 2	32	53	Ċ	-	111			3	YOR	7-1	H91H	923		•
96006	L 140ED	3	38	*	Ų.	2	121	9		>	4 0	1-A	41GH	r : 1		
2600t	SAT BA M	5	۳,	8	P)	.:	114		() H	•		1-4	н91+	SBA	ex/	
	* * * * * * * * * * * * * * * * * * *	> :	a.	M) (,	3. c	-	ရှာ (;e :		1-4	19 T	¥ ^ *		
566.5	X E4X147	3 5		ψ. K		. ,	121	o 0	7 6	> :	200	4 •	7. 19. 17. 17. 17. 17. 17. 17. 17. 17. 17. 17	O 6	X60 /X00	
	CLANSID	5	: :			٠,	-		,		2 0		2 2	2 5		
	SAN SIND	. 4	, F.	. 4		٠,			. u	נ י	2		30.1		*********	
90103	9AKERFLC	3	4 42 1 100		i C		119		4	1 38	200	1 - F	. x	200	1018/1018	
	PL* SPR	40	• •	5		٠.	116	w.	4		407	1-4	L 3 a	PSP	1027/102X	
	FRIANT	ک	.7	÷		مز	110	41	0 4	•	404	1-4	COK	103	1-3 x / 10 3 x	
9010é	PHX S HB	24	33	53	w,	••	111	53	11	,	VOR	1.3	H15H	PHX	103X/103X	
	SEAL SCH	40	33	-		ż.	11€	m >		3		1-4	F08	: Ts	104X/1C4X	
90166	DE 251.50	5	7	2		4	112	S			VOR	1-4	101	0.60	104X/104X	
	AEC BUF	٥ ا	•	in i	. 1	•	122		6	786	80	- F	н16н	86 L	104X/104X	
	S F TWTL	3	-	3			22	٠,		3	V O.	1-1	L.3.	SFO	105x/105x	
96111	COCHISE	r.,		21	0	2	501	s ·	27	٠.		1-4	1017	CIE	145X/105X	
21112	S F INTL	3 3		3.1		₽.	122	۰.				1-4	#16x	SFO	105x/	
51124	CATARILO	3	,	2 :	* (e i	119		9 6	3 :	X 0 8	7 .		4 . E	195x/105x	
471.0	1414141	<u>.</u> د	V 4		o s	. م	1		ž (. :	× 6	4 .		<u>.</u>	136x/106x	
;;	SIGIN ME	- d						٠.	<u></u>) (7 1	3 2 2	1964/1064	
	SORMAN	3		4		•	3 7 7					4-	20.7	2 2	196x/169x	
	JELTA MU	5	3	18	60	z	:12	30	11	:18	AC A	1-1	#5 I T	DTA	1C8X/1C8X	
	THERMAL	۲,	M)	37	•	2	116	50	4	>		1-1	H914	187	109x/109x	
	SAUSALIT	3	-	5		> .	122			>	0 A	1-4	#C1	SAU	1661/x631	
	WILSO CA	2 :	2,					n 1	40 ·	.	V .	7	H9 I I	ורנ ורנ	1107/1108	
27175	TORKE A	ر د و	· .	χ. c	. 4		131	n a	0 H	3 7	X 0 X	¥ •	3 6		1101	
90124	TOVELOCK	>		4		. 5	118			• 3	2	7 7	3 -	3 =	1124/1124	
90125	SAVIOTA	3		3.	•	. ,	123		*		YOR			0.0	112x/112x	
9¢15¢	FAIRFILD	Ë	ě	16		~	111	9	53	3		1-1	1967	FFU	113X/113X	
90127	GILA BEN	A 7	32	5.7		F	112		25	3	VOR	1-1	H16H	S.87	113x/113x	
9215	BOLDR CI	2	4) ₩)	7,		٠.	114	2		3	V OR	1-A	1917	513	114×/114×	
40150	WC*A	7 7	.,	41		; ;	114	36	80	,	VOR	1-1	1911	\$. >	115x/115x	
90138	S LAK CI	5	*	0	5	2 :	11	æ		3	20	Ţ.	H16H	SLC	115x/115x	
95131	OAKLAWO . 10 pro	٠ د د	<u>.</u>	4) (z :	122	P) {	57	> :	8 0 S	7-7	H20	OAK.	115x/115x	
9:132	LAS PEGA	2 3		20	- 4	z 2	222	5 6	2 6	.	X 0	7 7	1911	۲ م د د د	116x/116x	
96136	TICOURTH	; ;	5	2 6	, ,	: 2	7	2 4	, ,	> 3	F 0		TERMINAL STATE	F 25	11/8/	
90135	AVEVAL	3 5	1 17	3.0	; \$			200		. >	5 6			A C	1181/1181	
		į	;					1				,		•		

TABLE D-3
(Page 4 of 4)

SYSTER	LOCATION		Ē	EGUIP			50	۵		ليا	9116	PHEMI	•,		CHANNE	2
•	_	E .	141	110	3	_	LONG! TUDE	5	w		1	TYPE	VOLUME	LETTERS	OLD/NEW	2
90136	TONOPAH	2		8	. 5	2	117			3					1191/1104	
90137	EL TORO	Ü		•	0	7	117			-					1104/1104	
90138	SALIN MU	3		9	975	2	121								**************************************	
96139	BLY THE	2			5	2	114			3					1211/1211	
90140	FELLOWS	5		35 0	05 35	5 2	119	5		53.1	V O	4-I			122X/122X	
90141	PAGE	42		Š	5	*	111			3					123X/123X	
90142	COALDALE	ź		õ	: 0	2"	117			>					124X/1241	
90143	MISN BAY	3		ě	6.55	.	117			3					125X/125x	
90144	MYTON	5		0	÷	z	110			>					126X/126X	
90145	PARKER	5		<u>م</u>	9	4	114			3					126X/126X	
90106	RENO INT	Ž		m	<u>ئ</u>	2 2	119			3					126X/126x	
99147	3EALE	ŭ		-	4	ميز نند	121			3					25X/	
90148	SIERROPT	5		0	9	2	120			3					27X/ 27k	
90149	MCCLELLN	3		ě U	ت	≥	121			3					29X/ 29X	
90150	VISALIA	5		ii e	ە د	2: (4	119			>					31%/ 31%	
96151	SANTAMAR	3			7 0.	æ •	120			3					47X/ 47X	
90152	F1 0R0	C		4	2 2	يد ن	121			>					XCT /XCT	
90153	SANTAROS	Š		M 60	3,	2	122			:•					777.	
96154	LEWOORE	3		9	i,	•	119			.30					8CX/ 80x	
96155	PLACRVLL	Č		4	2	×	123			3					1001/1001	

FAA-RD-80-91 Appendix E

APPENDIX E

CHANNEL PLAN

This appendix contains a listing of the channel plan used in the initial assignment attempt.

TABLE E-1

CHANNEL PLAN
(Page 1 of 7)

Channel	C-Band (MHz)	L-Band (MHz)	L-Band (MHz)	VHF (MHz)	UHF (MHz)
17X	_		978	108.00	_
17Y	5031.0	1104	1104	108.05]
17XZ	5031.3	978	-	100.03	
18X	5031.6	979	979	108.10	334.10
18Y	5031.9	1105	1105	108.15	334.55
18XZ	5032.2	979	1105	100.13	334.33
19X	3032.2	[980	108.20] [
19Y	5032.5	1106	1106	108.25	_
19XZ	5032.8	980	1100	100.23	
20X	5033.1	981	981	108.30	334.10
20Y	5033.4	1107	1107	108.35	334.10
20XZ	5033.7	981	1107	100.55	334.33
21X	3055.7	-	982	108.40	
21Y	5034.0	1108	1108	108.45	_
21XZ	5034.3	982	-	106.45	_
22X	5034.6	983	983	108.50	329.90
22Y	5034.9	11/09	1109	108.55	
22XZ	5035.2		1	108.55	329.75
23X	3033.2	983	984	100.66	-
23X 23Y	5035.5	1110		108.66	
23XZ		1110	1110	108.65	-
23XZ 24X	5035.8	984	-	100.70	770 00
	5036.1	985	985	108.70	330.50
24Y	5036.4	1111	1111	108.75	330.35
24XZ	5036.7	985	-	-	-
25X	-	1	986	108.80	-
25Y	5037.0	1112	1112	108.85	-
25XZ	5037.3	986		-	
26X	5037.6	987	987	108.90	329.30
26Y	5037.9	1113	1113	108.95	329.15
26XZ	5038.2	987	- [-	-
27X	-	-	988	109.00	-
27Y	5038.5	1114	1114	109.05	-
27XZ	5038.8	988	•	 .	
28X	5039.1	989	989	109.10	331.40
28Y	5039.4	1115	1115	109.15	331.25
28XZ	5039.7	989	-	-	- 1
29X		-	990	109.20	- 1
29Y	5040.0	1116	1116	109.25	-
29XZ	5040.3	990	-	-	-
30X	5040.6	991	991	109.30	332.00
30Y	5040.9	1117	1117	109.35	331.85
30XZ	5041.2	991	- 1	-	- [

TABLE E-1

(Page 2 of 7)

Channel	C-Band (MHz)	L-Band (MHz)	L-Band (MH2)	VHF (MHz)	UHF (MHz)
31X	_	-	992	109.40	_
31Y	5041.5	1118	1118	109.45	-
31XZ	5041.8	992	-	-	- 1
32X	5042.1	993	993	109.50	332.60
32Y	5042.4	1119	1119	109.55	332.45
32XZ	5042.7	993	-	-	-
33X	-	-	994	109.60	-
33Y	5043.0	1120	1120	109.65	-
33XZ	5043.3	994	-	-	- 1
34X	5043.6	995	995	109.70	333.20
34Y	5043.9	1121	1121	109.75	333.05
34XZ	5044.2	995	-	-	- 1
35X	-	=i	996	109.80	-
35Y	5044.5	1122	1122	109.85	-
35XZ	5044.8	991	-	-	-
36X	5045.1	9 97	997	109.90	333.80
36Y	5045.4	1123	1123	109.95	333.65
36XZ	5045.7	997	-		-
37X	-		998	110.00	-
37Y	5046.0	1124	1124	110.05	- }
37XZ	5046.3	998	-	-	-
38X	5046.6	999	999	110.10	334.40
38Y	5046.9	1125	1125	110.15	334.25
38XZ	5047.2	999	-	-	- }
39X	-	-	1000	110.20	-
39Y	5047.5	1126	1126	110.25	-]
39XZ	5047.8	1000	-	-	- [
40X	5048.1	1001	1001	110.30	335.00
40Y	5048.4	1127	1127	110.35	334.85
40XZ	5048.4	1001	-	-	-
41X	-	-	1002	110.40	-
41Y	5049.0	1128	1128	110.45	-
41XZ	5049.3	1002	-	-	-
42X	5049.6	1003	1003	110.50	329.60
42Y	5049.9	1129	1129	110.55	329.45
42XZ	5050.2	1003	-	-	-
43X	-	-	1004	110.60	-
43Y	5050.5	1130	1130	110.65	-
43XZ	5050.8	1004	-		
44X	5051.1	1005	1005	110.70	330.20
44Y	5051.4	1131	1131	110.75	330.05
44XZ	5051.7	1005	-	-	-

TABLE E-1
(Page 3 of 7)

Channel	C-Band (Mfz)	L-Band (Miz)	L-Band (Miz)	VHF (MHz)	UHF (Miz)
45X	-	-	1006	110.80	_
45Y	5052.0	1132	1132	110.85	-
45XZ	5052.3	1006	-	-	-
46X	5052.6	1007	1007	110.90	330.80
46Y	\$052.9	1133	1133	110.95	330.65
46XZ	5053.2	1007	-	-	j -
47X	-	-	1008	111.00	j -
47Y	-	-	1134	111.05	-
47XZ	5053.5	1008	-	-	-
48X	5053.8	1009	1009	111.10	331.70
18A	5054.1	1135	1135	111.15	331.55
48XZ	5054.4	1009	-	-	-
49X	-	! -	1010	111.20	-
49Y	-	-	1136	111.25	-
19XZ	5054.7	1010	-	-	-
SOX	505 5.0	1011	1011	111.30	332.30
SOY	5055.3	1137	1137	111.35	332.15
50XZ	50 \$5.6	1011	-	-	-
SIX	-	-	1012	111.40	-
51Y	-] -	1138	111.45	-
51XZ	50\$5.9	1012	-	1 -	-
52 X	5056.2	1013	1013	111.50	332.90
52Y	5056.5	1139	1139	111.55	332.75
52XZ	5056.8	1013		-	-
53X	-	-	1014	111.60	-
53Y	-	-	1014	111.65	-
53XZ	5057.1	1014	-	-	-
S4X	5057.4	1015	1015	111.70	333.50
54Y	5057.7	1141	1141	111.75	333.35
S4XZ	5058.0	1015	-	•	-
\$5X	~	-	1016	111.80	-
55Y	-	-	1142	111.85	-
SSXZ	5058.3	1016	-	-	
S6X	5058.6	1017	1017	111.90	331.90
56Y	5058.9	1143	1143	111.95	330.95
S6XZ	5059.2	1017	1010	-	-
57X	~	-	1018	112.00	-
57Y	-	-	1144	112.05	-
S7XZ	5059.5	1018	1010	112.10	-
58X	~	-	1019	112.10	-
58Y	5050 0	1010	1145	112.15	-
58XZ 59X	\$0\$9.8	1019	1020	112 20	-
i v	~	-	1020	112.20	-
59Y	5060 1	1020	1146	112.25	-
S9XZ	5060.1	1020	-	-	-

TABLE E-1
(Page 4 of 7)

		· · · · · · · · · · · · · · · · · · ·	T		
Channel	C-Band (MHz)	L-Band (MHz)	L-Band (MHz)	VHF (MHz)	UHF (MH2)
•					
•		Ì		ł	1
•	}	ļ		•	•
70X	_	-	1157	112.30	-
70Y	-	-	1031	112.35	-
71X	•	-	1158	112.40	Ì
71Y	-	-	1032	112.45	
72X	-	-	1159	112.50	j
72Y	-	- .	1033	112.55	1
72XZ	5060.4	1159	-	-	-
73X	-	••	1160	112.60	-
73Y	-	-	1034	112.65	}
73XZ	5060.7	1160	-	-	-
74 X	-	-	1161	112.70	- '
74Y	-	-	1035	112.75	-
74 X Z	5061.0	1161	l -	-	-
75X	-	-	1162	112.80	-
75Y	-	{ -	1036	112.85	} -
75XZ	5061.3	1162	-	_	-
76X	-	-	1163	112.90	} -
76Y	-	-	1037	112.95) -
76 X Z	5061.6	1163	-	-	} -
77X	-	-	1164	113.00	-
7 7 Y	-	-	1038	113.05	-
77XZ	5061.9	1164	_] -	-
78X	-		1165	113.10	-
78Y	5062.2	1039	1039	113.15	-
78XZ	5062.5	1165	-	} -	<u> </u>
79X	ļ -) -	1166	113.20	j -
79Y	5062.8	1040	1166	113.20	
79XZ	5063.1	1166	-	-	_
80X	-	_	1167	113.30	_
80Y	5063.4	1041	1041	113.35	j -
80XZ	5063.7	1167	-	_	-
81X	-	-	1168	113.40	-
81Y	5064.0	1042	1042	113.45	-
81XZ	5064.3	1168	-	-	_
82X	-	-	1169	113.50	-
82Y	5064.6	1043	1043	113.55	
82XZ	5064.9	1169	-	_	_
83X	_	~	1170	113.60	1 -
83Y	5065.2	1044	1044	113.65	-
83XZ	5065.5	1170		-	l <u>-</u>

TABLE E-1
(Page 5 of 7)

Channe1	C-Band (MHz)	L-Band (MHz)	L-Band (MHz)	VHF (MHz)	UHF (MHz)
84X	-	-	1171	113.70	_
84Y	5065.8	1045	1045	113.75	-
84XZ	5066.1	1171	_	_	-
85X	-] -	1172	113.80	_
85Y	5066.4	1046	1046	113.85	_
85 X Z	5066.7	1172	-	-	-
86X	-	-	1173	113.90	
86Y	5067.0	1047	1047	113.95	_
86XZ	5067.3	1173	_	-	-
87X	-	-	1174	114.00	_
87Y	5067.6	1048	1048	114.05	_
87XZ	5067.9	1174	-	-	-
88X	-	_	1175	114.10	_
88Y	5068.2	1049	1049	114.15	_
88XZ	5068.5	1175	_	-	_
89X	_	_	1176	114.20	_
89Y	5068.8	1050	1050	114.25	[_ [
89XZ	5069.1	1176	_	_	_
90X	_		1177	114.30	_
90Y	5069.4	1051	1051	114.35	_
90XZ	5069.7	1177	1001	-	_
91X	-	1	1178	114.40	_
91Y	5070.0	1052	1052	114.45	
91XZ	5070.3	1178	1032	114.40	
92X] 50,0.5	1	1179	114.50	_
92Y	5070.6	1053	1053	114.55	
92XZ	5070.9	1179	1055	114.55	
93X	3070.3	11/3	1180	114.60	' <u> </u>
93Y	5070.2	1054	1054	114.65	_
93XZ	5070.5	1180	1054	114.03	
94X	3070.3	1100	1181	114.70	
94Y	5071.8	1055	1055	114.75	_ 1
94XZ	5072.1	1181	1055	114.75	_
95X	3072.1	1101	1182	114.80	_
95Y	5072.4	1056	1056	114.85	_ [
95XZ	5072.7	1182	1030	114.03	- 1
96X	3072.7	-	1183	114.90	
96Y	5073.0	1057	1057	114.90	_
96XZ	5073.3	1183		114.20	_]
97X	30/3.3		1184	115.00	<u> </u>
97X 97Y	5073.6	1058	1058	115.00	- 1
97XZ	5073.9			119,09	1
97XL 98X	30/3.9	1184	1185	115.10	-
98Y	5074.2	1050		1	-
	5074.5	1059	1059	115.15	- 1
98XZ	30/4.5	1185	- <u>[</u>	•	-

TABLE E-1
(Page 6 of 7)

Channel	C-Band (MHz)	L-Band (MHz)	L-Band (MHz)	VHF (MHz)	UHF (MHz)
99X	-	•	1186	115.20	_
99Y	5074.8	1060	1060	115.25	-
99XZ	5075.1	1186	_	_	-
100X	-	-	1187	115.30	-
100Y	5075.4	1061	1061	115.35	_
100XZ	5075.7	1187	_	-	-
101X	_	-	1188	115.40	_
101Y	5076.0	1062	1062	115.45	-
101XZ	5076.3	1188	_	-	-
102X	-	-	1189	115.50	-
102Y	5076.6	1063	1063	115.55	_
102XZ	5076.9	1189			_
103X		-	1190	115.60	_
103X 103Y	5077.2	1064	1064	115.65	_
103XZ	5077.5	1190			_
104X	30,7.3	1150	1191	115.70	_
104X 104Y	5077.8	1065	1065	115.75	_
1041 104XZ	5078.1	1191	-		_
104X2 105X	3076.1	1131	1192	115.80	_
105X 105Y	5078.4	1066	1066	115.85	_
1051 105XZ	5078.7	1192	1000	115.05	_
	30/0./	1192	1193	115.90	_
106X	5079.0	1067	1067	115.95	
106Y	5079.0	1193	1007	115.95	_
106XZ	50/9.3	1193	1	116.00	-
107X	-	-	1194		-
107Y	5079.6	1068	1068	116.05	-
107XZ	5079.9	1194	1105	116.10	-
108X	-	-	1195		-
108Y	5080.2	1069	1069	116.15	-
108XZ	5080.5	1195	1100	116 20	-
109X		-	1196	116.20	-
109Y	5080.8	1070	1070	116.20	_
109XZ	5081.1	1196		-	-
110X			1197	116.30	-
110Y	5081.4	1071	1071	116.35	-
110XZ	5081.7	1197			-
111X	.	-	1198	116.40	
111Y	5082.0	1072	1072	116.45	-
111XZ	5082.3	1198	-	-	-
112X	-	-	1199	116.50	-
112Y	5082.6	1073	1073	116.55	-
112XZ	5082.9	1199	- :	-	•

TABLE E-1
(Page 7 of 7)

Channel	C-Band (MHz)	L-Band (MHz)	L-Band (MHz)	VHF (MHz)	UHF (MHz)
113X	_	•	1200	116.60	
113Y	5083.2	1074	1074	116.65	_
113XZ	5083.5	1200	i -	-	- 1
114X	_	-	1201	116.70	-
114Y	5083.8	1075	1075	116.75	_
114XZ	5084.1	1201	j -	_] -
115X	_	-	1202	116.80	- 1
115Y	5084.4	1076	1076	116.85	- 1
115XZ	5084.7	1202	-	_	-
116X	-] -	1203	116.90] - [
116Y	5085.0	1077	1077	116.95	1 1
116XZ	5085.3	1203	-	-] -
117X	-	- '	1204	117.00	[- [
117Y	5085.6	1078	1078	117.05	-
117XZ	5085.9	1204	-	-	-
118X	} -	-	1205	117.10	J - j
118Y	5086.2	1079	1079	117.15	-
118XZ	5086.5	1205	-	-	-
119X	} -	} <u> </u>	1206	117.20) -
119Y	5086.8	1080	1080	117.25	1 - 1
119XZ	5087.1	1206	-	_	-
120X	-	_	1207	117.30	i - i
120Y .	5087.4	1081	1081	117.35	- 1
120XZ	5087.7	1207	-	-	-
121X	-	-	1208	117.40	-
121Y	5088.0	1082	1082	117.45] -]
121XZ	5088.3	1208	-	-	-
122X	-	-	1209	117.50	- 1
122Y	5088.6	1083	1083	117.55	- 1
122XZ	5088.9	1209	· -	-	- 1
123X	-	-	1210	117.60	-
123Y	5089.2	1084	1084	117.65	-
123XZ	5089.5	1210	-	-	-
124X	-	~	1211	117.70	i - 1
124Y	5089.8	1085	1085	117.75	-
124XZ	5090.1	1211	-	-	- 1
125X	-	-	1212	117.80	-
125Y	-		1086	117.85	-
125XZ	5090.4	1212	-	-	-
126X	-	-	1213	117.90	- [
126Y	-	~	1087	117.95	-
126XZ	5090.7	1213	-	-	- 1

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